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## **Convergence Estimates for Multidisciplinary Analysis and Optimization**

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# CONVERGENCE ESTIMATES FOR MULTIDISCIPLINARY ANALYSIS AND OPTIMIZATION

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**Abstract.** A quantitative analysis of coupling between systems of equations is introduced. This analysis is then applied to problems in multidisciplinary analysis, sensitivity, and optimization. For the sensitivity and optimization problems both multidisciplinary and single discipline feasibility schemes are considered. In all these cases a “convergence factor” is estimated in terms of the Jacobians and Hessians of the system, thus it can also be approximated by existing disciplinary analysis and optimization codes. The convergence factor is identified with the measure for the “coupling” between the disciplines in the system. Applications to algorithm development are discussed. Demonstration of the convergence estimates and numerical results are given for a system composed of two non-linear algebraic equations, and for a system composed of two PDEs modeling aeroelasticity.

**Key words.** convergence, MDO, sequential, Gauss-Seidel, adjoint, Hessian

**Subject classification.** Applied Numerical Mathematics

**1. Introduction.** In the last three years there have been a growing interest in the engineering community in the numerical solution of “multidisciplinary” (MD) problems [1]-[3]. A MD problem is defined in this work to be a problem which involves the solution of a set of equations which can be divided into at least two sets (disciplines). Three different MD problems are considered: the “Multidisciplinary Analysis” problem (MDA), the “Multidisciplinary Sensitivity” (Adjoint) problem (MDS), and the “Multidisciplinary Optimization” problem (MDO). The MDA problem is to solve a system of state equations, the MDS problem is to compute the sensitivity of some given quantity with respect to “design” parameters which appear in the state equations, and the MDO problem is to minimize a given cost-functional with respect to the design variables. Typically each set of state equations models a different physical process and therefore many times each set is dominated by different scales; the Jacobian of each set of equations is characterized by a different eigenvalue spectra resulting in a large and ill-conditioned problem. Also the MD problem introduces a practical difficulty of connecting large codes of different origin. Whenever possible (computational-wise) it is desirable to perform the computation in a “loosely coupled” scheme in which most of the computation is done in the disciplinary levels.

The recent effort in MDO is aiming at the development of new strategies and algorithms to solve the MD problems in a “tightly-coupled” approach. In some cases the optimization process is performed in the “system level” while the analysis and sensitivity analysis are performed in the disciplinary levels. Having the sensitivities of all the disciplines, the system optimization iteration convergence can be analyzed with classical methods developed for single discipline optimization. For such an approach this work is relevant only to the development of algorithms to solve the MDA and MDS problems. References [1]-[3] summarize most of the work done so far in MDO. R.J. Balling and J. Sobieski [4] propose several multi-level algorithms for the solution of MDO problems in which the design process is decomposed into the disciplinary levels.

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E.J. Cramer et. al. [5] propose three fundamental formulations to MDO based on feasibility requirements: Multidisciplinary Feasible (MDF), Individual Discipline Feasible (IDF), and All-At-Once (AAO). These formulations were applied by G.R. Shubin [6] to aeroelasticity and it is reported that in general the less feasible formulation, AAO, was the most efficient in practice.

The classical approach to such problems is the sequential (“one-at-a-time”) approach; solve each disciplinary problem separately, while freezing the variables of the other disciplines. Up-to-date the sequential approach is used in applications to solve multidisciplinary optimization problems, for example in aircraft design (e.g.,[7]). The sequential approach has the advantage that it is the simplest to apply since typically there is a great deal of information and experience on numerical methods for the solution of each of the disciplinary problems. However, in many cases such an approach is undesirable since it might not converge to the MD solution at all [8], and in some other cases it might converge to the solution but slowly, requiring numerous disciplinary solutions and exchange of data between the disciplines at each MD iteration. The sequential approach is known in iterative methods for solving algebraic equations as the Gauss-Seidel algorithm (for example [9] p.508), i.e., each of the equations in the system is solved separately for one variable while freezing the variables of the other equations. Therefore, in this paper such an approach will be called “a Generalized Gauss-Seidel” (GGS) approach. The GGS approach has a parallel version in which the disciplinary problems are solved separately in parallel rather than sequentially. This scheme is known in iterative methods for solving algebraic equations as the Jacobi algorithm and therefore in this paper such an approach will be called the “Generalized Jacobi” (GJ) approach.

Qualitative predictions of the GGS convergence for an MDO problem were done in [10], where it was shown that the MD Hessian determines the coupling in a static aeroelastic optimization problem. Local mode analysis of the MD Hessian was performed to prove that for the non-smooth error mode components the problem has very weak coupling between aerodynamic design and structural design and therefore it predicts that a sequential approach will be efficient for that problem.

In this paper, a quantitative convergence analysis is developed for the GGS (sequential), and GJ (parallel), schemes applied to MDA, MDS, and MDO problems. An upper bound for the convergence rate of the GGS scheme is estimated by the maximal singular value of a “convergence matrix”,  $\mathcal{M}$ , that is given in terms of the Jacobians and Hessians of the problem. In problems governed by PDEs the convergence matrix is an operator (typically non-differential) which determines the “coupling” between the disciplines in the system. We claim that these operators have a fundamental role in the mathematical theory of MDO and we give an explicit analysis of these operators for an aeroelastic model problem (Sec. 6). The motivation behind that analysis is to be able to predict a-priori which of the subsystems in a given MD problem are “loosely coupled” in the sense that a GGS approach will be computationally efficient when applied to the solution of these sub-systems. The estimates allow to use mathematical theory, for example theory of Partial Differential Equations (PDEs) in the differential level or linear algebra in the discrete level, to estimate these convergence factors. Since the estimates are given in terms of the Jacobians and Hessians of the MD system they can be approximated by existing analysis and optimization disciplinary codes. Throughout the paper we assume that the problems at hand are well-posed and that there exists a unique solution; only the issue of numerical convergence to the solution of these problems is addressed.

Demonstration of the convergence estimates and numerical results are given for a system composed of two non-linear algebraic equations and for a system composed of two PDEs modeling aeroelasticity. The numerical results are compatible with the analytical estimates.

Throughout the paper the following notation is used (some of the notation is taken from [11]):

$A_i$  - Analysis of system  $i$ ,

$S_i$  - Sensitivity (Adjoint) analysis of system  $i$ ,

$O_i$  - Optimization of system  $i$ ,

$(Z_1, Z_2)$  - Single execution of  $Z_1$  followed by  $Z_2$ ,

$[Z_1, Z_2]$  - Nested execution of  $Z_1$  followed by  $Z_2$ ,

$[Z_1 || Z_2]$  - Nested execution of  $Z_1$  and  $Z_2$  in parallel (freezing the coupling information at each execution).

For example,  $(A_1, A_2)$  denotes the analysis of system 1 followed by the analysis of system 2, and  $[O_1(A_1, S_1) || O_2(A_2, S_2)]$  denotes a nested execution of solving in parallel the MDO problem composed of disciplines 1 and 2 (freezing the coupling information at each execution), where in each disciplinary optimization problem there is a sequential application of the disciplinary analysis and sensitivity analysis.

The paper is divided into sections as follows:

In Secs.2, 3, and 4 the MDA, MDS (Adjoint), and MDO problems are treated respectively.

In Sec.5 the theory is demonstrated on a non-linear algebraic set of two equations.

In Sec.6 the theory is demonstrated on a set of two PDEs modeling static aeroelastic system.

In Sec. 7 discussion and concluding remarks are made followed by the list of references.

Appendix A presents the norm used throughout the paper.

Appendix B gives a short presentation of the sensitivity equation and the adjoint methods.

Appendix C gives the proof of Lemma 1.

Appendix D gives the Fourier analysis of the aeroelastic problem which is discussed at Sec. 6.

**2. The Multidisciplinary Analysis Problem.** In a Multidisciplinary Analysis (MDA) problem a coupled system of equations (typically PDEs) is solved,

$$(2.1) \quad R_j(Q_1, \dots, Q_N) = 0 \quad ; \quad j = 1, \dots, N,$$

where  $R_j$  denotes the  $j$ 'th state equation and  $Q_k$  denotes the  $k$ 'th state variable. If  $R_j$  is a differential operator then in the discrete level each of the equations  $R_j$  is composed of a system of  $N_j$  algebraic equations and each of the state variables  $Q_j$  is a vector of the size  $N_j$ .

The notation  $(A_{k_1}, A_{k_2}, \dots, A_{k_N})$  is used to denote a GGS iteration for a MD system which is composed of  $N$  state equations, where the integers  $(k_1, k_2, \dots, k_N)$  are a permutation of  $(1, 2, \dots, N)$ ; equation  $k_1$  is solved first for the state variable  $Q_{k_1}$ , then equation  $k_2$  for  $Q_{k_2}$  and so on. The notation  $(A_{k_1} || A_{k_2} || \dots || A_{k_N})$  is used to denote a GJ iteration in which all the equations are solved in parallel. Note that in the GGS case there are  $N!$  different sequences of iterations depending on the order of solutions while in the GJ case there is only one choice.

For simplicity a two disciplines system will be considered from here on:

$$(2.2) \quad \begin{aligned} R_1(Q_1, Q_2) &= 0 \\ R_2(Q_1, Q_2) &= 0. \end{aligned}$$

The system (2.2) can be solved in a *tightly coupled* iterative algorithm for example by Newton's method or by an exact solver for the full system. One difficulty with a tightly coupled solution is that the full problem is typically ill-conditioned; even if each of the disciplinary problems is well-conditioned (by preconditioning for example), the Jacobian's eigenvalues of one discipline will typically be different than the eigenvalues of the second discipline. Another practical difficulty with this approach is the need to join together the analysis codes of the different disciplines.

## 2.1. A Generalized Gauss-Seidel (GGS) Scheme.

### Definition:

A GGS iteration for the two discipline system (2.2) is defined by the following procedure (see Fig.(1)):

#### Scheme 1.1

Starting with an approximation  $(Q_1^n, Q_2^n)$  (from here on the notation  $^n$  will be omitted, for example  $Q_1 \equiv Q_1^n$ ),

1. Solve for  $Q_1^{n+1}$  the equation  $R_1(Q_1^{n+1}, Q_2) = 0$ ,
2. Solve for  $Q_2^{n+1}$  the equation  $R_2(Q_1^{n+1}, Q_2^{n+1}) = 0$ .

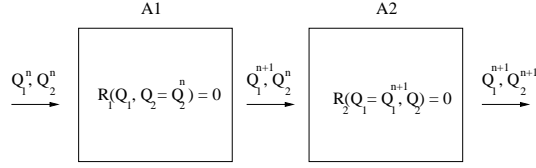


FIG. 1. GGS Iteration for the MDA Problem:  $(A_1, A_2)$ .

In some cases the GGS sequential algorithm might require many MD iterations thus it might result with a much higher computational cost than a tightly coupled solution. In such cases there is also a practical difficulty since each of the disciplinary solutions is computed with a different code, thus each GGS iteration requires information interchange between these codes.

However, in some cases the GGS scheme converges efficiently to the MD solution. In the rest of this section the condition for convergence of GGS iteration is analyzed and a quantitative estimate of its convergence rate,  $\mu_a$ , is derived. This might serve as a tool to develop algorithms in complex systems where possibly only a subset of the system may require tightly coupled solutions; for a system composed of more than two disciplines it is possible to have a subsystem which is solved in a tightly coupled manner. For example, in a three disciplines system it is possible to define the MD iteration  $(A_1, [A_2, A_3])$ , i.e., solve state equation number one for  $Q_1$  and then solve tightly coupled the state equations number two and three for  $Q_2$  and  $Q_3$ . It is possible that different sequences of GGS iterations result in different error reduction, e.g.,  $(A_1, A_2, A_3)$  versus  $(A_1, A_3, A_1)$ . In that case we would like to analyze which of the sequences results in a maximum error reduction.

**2.1.1. Linearization.** A linear relationship between errors and residuals for the system of state equations is assumed. In the two disciplines system such a relationship can be written in a matrix form as

$$(2.3) \quad \begin{pmatrix} R_{1,Q_1} & R_{1,Q_2} \\ R_{2,Q_1} & R_{2,Q_2} \end{pmatrix} \begin{pmatrix} \bar{Q}_1 \\ \bar{Q}_2 \end{pmatrix} = - \begin{pmatrix} R_1 \\ R_2 \end{pmatrix}$$

where in general the quantities  $R_{ij}$  depend on the state variables  $\vec{Q}$  and where  $\bar{Q}$  and  $\bar{R}$  denote the errors and residuals at iteration  $n$  respectively. The block matrices  $R_{i,Q_j}$  are dominated by the Jacobian  $\frac{\partial R_i}{\partial Q_j}$  and are equal to it in linear systems. We will assume that the block diagonal matrices in (2.3) are invertible.

Note that in the differential level the quantities  $\frac{\partial R_i}{\partial Q_j}$  should be understood as the Fréchet derivative of a function space entity,  $R_i \in \mathcal{W}$ , with respect to another,  $Q_j \in \mathcal{X}$ . Such a derivative is an operator from  $\mathcal{X}$

to  $\mathcal{W}$ :

$$R_{i,Q_j} : \mathcal{X} \rightarrow \mathcal{W}.$$

**2.1.2. The GGS Iteration in terms of the System Jacobian.** Starting with the states  $Q_1$  and  $Q_2$  the GGS iteration (see scheme 1.1) can be written as

$$(2.4) \quad \begin{aligned} Q_1^{n+1} &= Q_1 + \tilde{Q}_1 \\ Q_2^{n+1} &= Q_2 + \tilde{Q}_2 \end{aligned}$$

where  $\tilde{Q}_1$  and  $\tilde{Q}_2$  satisfy the following system of equations:

$$(2.5) \quad \begin{pmatrix} R_{1,Q_1} & 0 \\ R_{2,Q_1} & R_{2,Q_2} \end{pmatrix} \begin{pmatrix} \tilde{Q}_1 \\ \tilde{Q}_2 \end{pmatrix} = - \begin{pmatrix} R_1 \\ R_2 \end{pmatrix}.$$

## 2.2. Convergence Analysis.

### Definition:

The *convergence factor* for the analysis problem (2.2),  $\mu_a$ , is defined to be the maximum of the disciplinary error reduction in the state variables as a result of one application of the MD iteration:

$$(2.6) \quad \mu_a = \max \left\{ \frac{\|\bar{Q}_1^{n+1}\|}{\|\bar{Q}_1\|}, \frac{\|\bar{Q}_2^{n+1}\|}{\|\bar{Q}_2\|}, \dots, \frac{\|\bar{Q}_N^{n+1}\|}{\|\bar{Q}_N\|} \right\}.$$

In non-linear problems the convergence factor depends on the state variables,  $\mu_a = \mu_a(\vec{Q})$ .

For small values of  $\mu_a$  the MDA problem can be solved with a small number of GGS iterations. The higher the value of  $\mu_a$  (but still smaller than one) the more GGS iterations required to solve the MDA problem.

The convergence of the loosely coupled iteration is determined by the map  $T$  which relates the error,  $\vec{e}$ , to the error after application of a MD iteration,  $\vec{e}^{n+1}$ :

$$(2.7) \quad T : \vec{e} \rightarrow \vec{e}^{n+1}.$$

In the following the map  $T$  is studied for the GGS and GJ iterations for the solution of the MDA problem. We first find the explicit form of the map  $T$  (locally) and then take its maximal singular value,  $\sigma_1(T)$ , as the measure of its  $L^2$  norm (see Appendix A). The error decrease as a result of an MD iteration is estimated

$$(2.8) \quad \|\vec{e}^{n+1}\| \leq \sigma_1(T) \|\vec{e}\|.$$

We claim that any MD iteration, including the sequential GGS (which is characterized by a map  $T$  defined in (2.7)) converges to the MD solution if and only if  $\sigma_1(T^n) < (1 - \epsilon)$ , for  $n > N$  where  $N$  is some integer greater than unity, and  $\epsilon$  is some real positive number smaller than unity:  $0 < \epsilon < 1$ .

### Lemma 1:

For a two states system (2.2), starting with errors  $\bar{Q}_1$  and  $\bar{Q}_2$  in the state variables and assuming that the errors satisfy the quasi-linear approximation (2.3), a GGS sequential iteration  $(A_1, A_2)$  results in the following error relations:

$$(2.9) \quad \begin{aligned} \bar{Q}_1^{n+1} &= \left( R_{1,Q_1}^{-1} R_{1,Q_2} (R_{2,Q_2}^{n-1})^{-1} R_{2,Q_1}^{n-1} \right) \bar{Q}_1 \\ \bar{Q}_2^{n+1} &= \left( R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} R_{1,Q_2} \right) \bar{Q}_2. \end{aligned}$$

The proof is given in Appendix C.

**2.2.1. The Convergence Matrix.** The *convergence matrix* for a two discipline system is defined by

$$(2.10) \quad \mathcal{M}_a = R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} R_{1,Q_2}.$$

In terms of the convergence matrix the errors in the state variables are given by:

$$(2.11) \quad \bar{Q}_2^{n+1} = \left( \prod_{k=n}^0 \mathcal{M}_a^k \right) \bar{Q}_2^0$$

$$(2.12) \quad \bar{Q}_1^{n+1} = -(R_{1,Q_1})^{-1} R_{1,Q_2} \left( \prod_{k=n-1}^0 \mathcal{M}_a^k \right) \bar{Q}_2^0.$$

Defining a new variable for discipline 1:

$$z_1 = -R_{2,Q_2}^{-1} R_{2,Q_1} Q_1$$

we get that the error reduction in  $z_1$  is identical to the error reduction in  $Q_2$  at all iterations and therefore we conclude that the convergence matrix determines the total error reduction in the system.

The local error at iteration  $n$  is bounded by (the same relation holds for  $z_1$ )

$$(2.13) \quad \|\bar{Q}_2\|^{n+1} \leq \|\mathcal{M}_a\| \|\bar{Q}_2\|.$$

**2.3. Connection with Classical Gauss-Seidel and Jacobi Methods.** The iteration (2.4-2.5) is a generalization of Gauss-Seidel (GS) iteration to systems of equations. When applying GS iteration to solve an algebraic system of equations  $Ax = b$  where  $A$  is a matrix and  $x$  and  $b$  are vectors with proper dimensions, then a GS iteration has the form

$$(2.14) \quad Mx^{n+1} = Nx + b$$

where  $M = D + L$ ,  $N = -U$ , and  $D$ ,  $L$ , and  $U$  are the diagonal, lower triangular, and upper triangular of  $A$  respectively. The convergence of GS iteration is determined by the spectral radius  $\rho(M^{-1}N)$  ([9] p.508):

**Theorem 1:**

Suppose  $b \in \mathbb{R}$  and  $A = M + N \in \mathbb{R}^{n \times n}$  is nonsingular. If  $M$  is nonsingular and the spectral radius of  $M^{-1}N$  satisfies the inequality  $\rho(M^{-1}N) < 1$ , then the iterates  $x^{(k)}$  defined by  $Mx^{(k+1)} = Nx^{(k)} + b$  converge to  $x = A^{-1}b$  for any starting vector  $x^{(0)}$ .

**Generalized Gauss-Seidel**

The MD iteration defined by (2.4-2.5) is a GS iteration (2.14) with

$$(2.15) \quad M = \begin{pmatrix} R_{1,Q_1} & 0 \\ R_{2,Q_1} & R_{2,Q_2} \end{pmatrix} \quad ; \quad N = - \begin{pmatrix} 0 & R_{1,Q_2} \\ 0 & 0 \end{pmatrix}.$$

The matrix  $M^{-1}N$  is given by

$$(2.16) \quad M^{-1}N = \begin{pmatrix} 0 & R_{1,Q_1}^{-1} R_{1,Q_2} \\ 0 & R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} R_{1,Q_2} \end{pmatrix}.$$

By theorem 1 the iteration (2.4-2.5) converges if  $\rho(M^{-1}N) < 1$  where

$$(2.17) \quad \rho(M^{-1}N) = \rho(R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} R_{1,Q_2}).$$

Note that the expression in (2.17) is the convergence matrix (2.10).

### **Generalized Jacobi**

The sequential iteration  $(A_1, A_2)$  can be replaced by a parallel version  $(A_1 \| A_2)$  where  $A_1$  is solved in parallel to  $A_2$ . This iteration will be called a “Generalized Jacobi” (GJ) MD iteration, since it is a Jacobi iteration with

$$(2.18) \quad M = \begin{pmatrix} R_{1,Q_1} & 0 \\ 0 & R_{2,Q_2} \end{pmatrix} \quad ; \quad N = - \begin{pmatrix} 0 & R_{1,Q_2} \\ R_{2,Q_1} & 0 \end{pmatrix}.$$

The matrix  $M^{-1}N$  is given by

$$(2.19) \quad M^{-1}N = \begin{pmatrix} 0 & R_{1,Q_1}^{-1} R_{1,Q_2} \\ R_{2,Q_2}^{-1} R_{2,Q_1} & 0 \end{pmatrix}.$$

According to theorem 1 the GJ iteration converges if  $\rho(M^{-1}N) < 1$ .

Eq. (2.19) implies that the asymptotic convergence rate of the GJ scheme is the square-root of the GGS, i.e., the sequential (GGS) approach requires less MD iterations than the parallel (GJ) to converge.

In a similar manner other iterative schemes can be generalized to MD systems (e.g., Richardson, Kaczmarz, Etc.). Also, it is possible to apply generalized acceleration techniques developed for systems of equations to MD systems, for example, SOR of GS can be applied to accelerate the numerical convergence of the GGS scheme; in that case the update will depend on the SOR parameter,  $\omega$ , and one should choose the SOR parameter,  $\omega$ , such that  $\min_{\omega} \|\mathcal{M}_a(\omega)\|$ . Extension of this work to acceleration of MDO schemes will be discussed elsewhere.

**3. The Multidisciplinary Sensitivity (Adjoint) Problem.** In a Multidisciplinary Sensitivity Analysis (MDS) problem the sensitivities of the states or of a cost functional with respect to disciplinary “design variables”,  $(b_1, \dots, b_M)$ , are computed. In the discrete level each  $b_k$  is a vector of length  $M_k$ . The system (2.1) now includes the design variables and have the following form

$$(3.1) \quad R_j(Q_1, \dots, Q_N, b_k) = 0 \quad ; \quad j = 1, \dots, N \quad ; \quad k \in \mathcal{C}_j$$

where  $\mathcal{C}_j$  is a subset of the integers of  $\{1, \dots, M\}$ .

In this section the problem of computing sensitivities of a cost functional,  $I$ , with respect to the design variables is addressed. The cost functional,  $I$ , is a mapping between a vector space (a Hilbert space in the PDE level) to the real numbers and is possibly dependent on all the variables:

$$I = I(Q_1, \dots, Q_N, b_1, \dots, b_M).$$

The “MDS problem” is the computation of the sensitivities:

$$(3.2) \quad (g_1, \dots, g_M) \equiv \left( \frac{dI}{db_1}, \dots, \frac{dI}{db_M} \right).$$

As in the previous section, for the sake of simplicity, the discussion will be restricted to the following system of equations which is related with aeroelasticity:

$$(3.3) \quad \begin{aligned} R_1(Q_1, Q_2, b_1) &= 0 \\ R_2(Q_1, Q_2, b_2) &= 0. \end{aligned}$$



In the aeroelastic application  $Q_1$  stands for the flow variables,  $Q_2$  for the structural deflection,  $b_1$  the aerodynamic shape and  $b_2$  for the structural rigidity (see Sec.5). Similar analysis can be done to any other MD system.

Since there is only a single quantity as an “output” (the cost functional  $I$ ) and many “inputs” (the design variables  $\{b_k\}_{k=1}^M$ ) the most efficient method to compute the sensitivities in such a case is the *adjoint method*. A brief explanation of the adjoint method is given in appendix B (for a more rigorous treatment of the subject see for example [12]).

Since the Jacobian in the adjoint equation is the adjoint of the Jacobian in the sensitivity equations (obtained by direct differentiation) the convergence estimates for both are identical (see Appendix B).

**3.1. Adjoint Formulation.** The derivatives of the cost functional with respect to the design variables (sensitivity gradients) are given by

$$(3.4) \quad \begin{pmatrix} g_1 \\ g_2 \end{pmatrix} = \begin{pmatrix} \frac{\partial I}{\partial b_1} + \left(\frac{\partial R_1}{\partial b_1}\right)^* \Lambda_1 + \left(\frac{\partial R_2}{\partial b_1}\right)^* \Lambda_2 \\ \frac{\partial I}{\partial b_2} + \left(\frac{\partial R_1}{\partial b_2}\right)^* \Lambda_1 + \left(\frac{\partial R_2}{\partial b_2}\right)^* \Lambda_2 \end{pmatrix},$$

where the Lagrange multipliers,  $\Lambda_1$  and  $\Lambda_2$ , satisfy the following “adjoint” or “costate” equations” ( $I_{b_k}$  denotes  $\frac{\partial I}{\partial b_k}$  and  $R_{i,Q_j}^*$  denotes  $\left(\frac{\partial R_i}{\partial Q_j}\right)^*$ ):

$$(3.5) \quad \begin{aligned} P_1(\Lambda_1, \Lambda_2, Q_1, Q_2, b_1, b_2) &= I_{b_1} + R_{1,Q_1}^* \Lambda_1 + R_{2,Q_1}^* \Lambda_2 = 0 \\ P_2(\Lambda_1, \Lambda_2, Q_1, Q_2, b_1, b_2) &= I_{b_2} + R_{1,Q_2}^* \Lambda_1 + R_{2,Q_2}^* \Lambda_2 = 0. \end{aligned}$$

Note that the costate equations are linear in the costate variables,  $\vec{\Lambda}$ , with non-constant coefficient that depend on the state and design variables,  $\vec{Q}$  and  $\vec{b}$  respectively.

**3.2. Multidisciplinary Feasible Sensitivity Solution:**  $[S_1, S_2] \equiv [S_1[A_1, A_2], S_2[A_1, A_2]]$ . Each of the disciplinary sensitivity calculations is assumed to be done on a MDA solution as shown in Fig.2. Since the state equations are assumed to be solved prior to the solution of the MDS problem only the system (3.5) is considered. In terms of the notations  $R_{ij}$ , used in the previous section, the system of error equations is given by

$$(3.6) \quad \begin{pmatrix} R_{1,Q_1}^* & R_{2,Q_1}^* \\ R_{1,Q_2}^* & R_{2,Q_2}^* \end{pmatrix} \begin{pmatrix} \bar{\Lambda}_1 \\ \bar{\Lambda}_2 \end{pmatrix} = - \begin{pmatrix} P_1 \\ P_2 \end{pmatrix}$$

where  $P_1$  and  $P_2$  are the residuals of the system (3.5) at iteration  $n$ . A GGS iteration and the convergence factor are defined in similar to the MDA case and the convergence factor is given by a similar formula.

Notation.

The notation for a GGS iteration for a MD adjoint problem which is composed of  $N$  costate equations is  $(S_{k_1}, S_{k_2}, \dots, S_{k_N})$  where the indices should be understood as in the analysis case.

#### Scheme 2.1: A GGS Adjoint Iteration

A *GGS* iteration of the two discipline system (3.5) is given by the following two steps, starting with an approximation  $(\Lambda_1, \Lambda_2)$  and keeping the state  $(Q_1^*, Q_2^*)$  and the design  $(b_1, b_2)$  variables fixed:

1. Solve for  $\Lambda_1^{n+1}$  the equation  

$$P_1(\Lambda_1^{n+1}, \Lambda_2 = \Lambda_2^n, Q_1^*, Q_2^*, b_1, b_2) = 0$$

2. Solve for  $\Lambda_2^{n+1}$  the equation

$$P_2(\Lambda_1 = \Lambda_1^n, \Lambda_2^{n+1}, Q_1^*, Q_2^*, b_1, b_2) = 0.$$

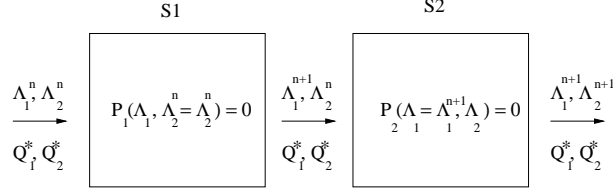


FIG. 2. MD Feasible Sensitivity Solution:  $[S_1, S_2] \equiv [S_1[A_1, A_2], S_2[A_1, A_2]]$ .

**Lemma 2.1:**

For a two states system (3.6), starting with errors  $\bar{\Lambda}_1$  and  $\bar{\Lambda}_2$  in the costate variables and assuming fixed states, a GGS iteration of the adjoint problem  $(S_1, S_2)$  results in the following relations for errors reduction:

$$(3.7) \quad \begin{aligned} \bar{\Lambda}_1^{n+1} &= \left[ R_{1,Q_1}^{-*} R_{2,Q_1}^* (R^{n-1})_{2,Q_2}^{-*} (R^{n-1})_{1,Q_2}^* \right] \bar{\Lambda}_1 \\ \bar{\Lambda}_2^{n+1} &= \left[ R_{2,Q_2}^{-*} R_{1,Q_2}^* R_{1,Q_1}^{-*} R_{2,Q_1}^* \right] \bar{\Lambda}_2. \end{aligned}$$

The proof is identical to the proof of Lemma 1.

The convergence matrix for the sensitivity problem is defined by

$$(3.8) \quad \mathcal{M}_{a^*} = R_{2,Q_2}^{-*} R_{2,Q_1}^* R_{1,Q_1}^{-*} R_{1,Q_2}^*.$$

**3.3. Single Discipline Feasible Sensitivity Solution:**  $[S_1(A_1), S_2(A_2)]$ . In this section the convergence factor for the combined computation of analysis and sensitivity, of a MD system as shown in Fig.3, is estimated.

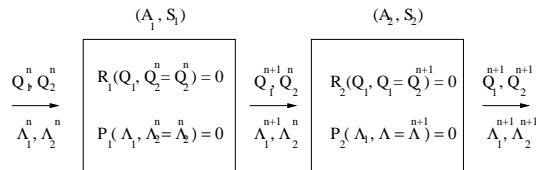


FIG. 3. Single Discipline Feasible Sensitivity Solution:  $[S_1(A_1), S_2(A_2)]$ .

Scheme 2.2: A GGS Analysis and Adjoint and Iteration

The process which is under consideration is summarized by the following two steps iteration, starting with an initial approximation  $(Q_1^0, Q_2^0, \Lambda_1^0, \Lambda_2^0)$  iteration  $n + 1$  (where  $n > 0$ ) is given by:

Step 1:  $(A_1, S_1)$ ,

1. Solve for  $Q_1^{n+1}$  the state equation,

$$R_1(Q_1^{n+1}, Q_2 = Q_2^n, b_1) = 0.$$

2. Solve for  $\Lambda_1^{n+1}$  the costate equation,

$$P_1(\Lambda_1^{n+1}, \Lambda_2 = \Lambda_2^n, Q_1^{n+1}, Q_2^n, b_1, b_2) = 0.$$

Step 2:  $(A_2, S_2)$ ,

1. Solve for  $Q_2^{n+1}$  the state equation,

$$R_2(Q_1 = Q_1^{n+1}, Q_2^{n+1}, b_2) = 0.$$

2. Solve for  $\Lambda_2^{n+1}$  the costate equation,

$$P_2(\Lambda_1 = \Lambda_1^n, \Lambda_2^{n+1}, Q_1^{n+1}, Q_2^{n+1}, b_1, b_2) = 0.$$

### **Definitions:**

The *sensitivity convergence factor*,  $\mu_s$ , is defined to be the error reduction in the costate variables as a result of one GGS analysis and adjoint iteration as defined by Scheme 2.2.

### **Lemma 2.2:**

For a two states system (3.3), starting with errors  $\bar{\Lambda}_1$  and  $\bar{\Lambda}_2$  in the costate variables and assuming that the errors in the state variables satisfy the quasi-linear approximation (2.3), then a GGS iteration  $((A_1, S_1), (A_2, S_2))$  for the solution of the MDS problem results in the following errors reduction:

$$\begin{aligned}\bar{e}_1^{n+1} &= S_{11}^{-1} S_{12} (S_{22}^{n-1})^{-1} S_{21}^{n-1} \bar{e}_1 \\ \bar{e}_2^{n+1} &= S_{22}^{-1} S_{21} S_{11}^{-1} S_{12} \bar{e}_2.\end{aligned}$$

where

$$(3.9) \quad S_{ij} = \begin{pmatrix} R_{i,Q_j} & 0 \\ P_{i,Q_j} & P_{i,\Lambda_j} \end{pmatrix}$$

and the errors  $\bar{e}_i = (\bar{Q}_i, \bar{\Lambda}_i)$ .

### **Proof:**

The GGS analysis and adjoint iteration is updating the variables  $(Q_1, \Lambda_1)$  and  $(Q_2, \Lambda_2)$  with the quantities  $\tilde{e}_1$  and  $\tilde{e}_2$  respectively which satisfy the following equation

$$(3.10) \quad - \begin{pmatrix} r_1 \\ r_2 \end{pmatrix} = \begin{pmatrix} S_{11} & 0 \\ S_{21} & S_{22} \end{pmatrix} \begin{pmatrix} \tilde{e}_1 \\ \tilde{e}_2 \end{pmatrix}$$

where  $r_i = (R_i, P_i)$ .

We brought the MDS problem into the same form as the MDA problem (see Eqs. (2.3) and (2.5)) with the changes  $R_{ij} \rightarrow S_{ij}$ ,  $R_j \rightarrow r_j$  and  $\bar{Q} \rightarrow \bar{e}$ , and  $\bar{Q} \rightarrow \bar{e}$ . Using Lemma 1 we conclude that

$$(3.11) \quad \begin{aligned}\bar{e}_1^{n+1} &= S_{11}^{-1} S_{12} (S_{22}^{n-1})^{-1} S_{21}^{n-1} \bar{e}_1 \\ \bar{e}_2^{n+1} &= S_{22}^{-1} S_{21} S_{11}^{-1} S_{12} \bar{e}_2.\end{aligned}$$

□

The *convergence matrix* of a GGS sensitivity (adjoint) iteration,  $(S_1(A_1), S_2(A_2))$ , is defined by

$$(3.12) \quad \mathcal{M}_s = S_{22}^{-1} S_{21} S_{11}^{-1} S_{12}.$$

The convergence factor for the iteration  $(S_1(A_1), S_2(A_2))$  is bounded from above by the maximum singular value of  $\mathcal{M}_s$  or equivalently by the square-root of the spectral radius of  $\mathcal{M}_s^* \mathcal{M}_s$ :

$$(3.13) \quad \mu_s \leq \rho^{\frac{1}{2}}(\mathcal{M}_s^* \mathcal{M}_s).$$

Note that the block diagonal terms in the convergence matrix,  $\mathcal{M}_s$ , are  $\mathcal{M}_a$  and  $\mathcal{M}_{a^*}$ :

$$(3.14) \quad \mathcal{M}_s = \begin{pmatrix} \mathcal{M}_a & 0 \\ \mathcal{M}_{as} & \mathcal{M}_{a^*} \end{pmatrix}.$$

The eigenvalues of  $\mathcal{M}_s$  are equal to the eigenvalues of  $\mathcal{M}_a$  and  $\mathcal{M}_{a^*}$ . However the maximal singular value of  $\mathcal{M}_s$  is different than that of  $\mathcal{M}_a$  and  $\mathcal{M}_{a^*}$  and therefore the convergence rate of the scheme  $[S_1(A_1), S_2(A_2)]$  is possibly different than that of  $[S_1[A_1, A_2], S_2[A_2, A_2]]$ .

**4. The Multidisciplinary Optimization Problem.** In a Multidisciplinary Optimization (MDO) problem the minimum of a given cost functional with respect to the disciplinary design variables,  $(b_1, \dots, b_M)$ , is computed:

$$(4.1) \quad \min_{(b_1, \dots, b_M)} I(Q_1, \dots, Q_N, b_1, \dots, b_M),$$

subject to the MD state equations:

$$R_j(Q_1, \dots, Q_N, b_k) = 0 \quad ; \quad j = 1, \dots, N \quad ; \quad k \in \mathcal{C}_j.$$

As in the previous sections, for the sake of simplicity, the discussion will be restricted to the following problem which is related with aeroelasticity:

$$(4.2a) \quad \min_{(b_1, b_2)} I(Q_1, Q_2, b_1, b_2)$$

subject to

$$(4.2b) \quad \begin{aligned} R_1(Q_1, Q_2, b_1) &= 0 \\ R_2(Q_1, Q_2, b_2) &= 0. \end{aligned}$$

The adjoint formulation is used for the derivation of the sensitivity gradients (see Sec. 3.1 and Appendix B).

**4.1. Multidisciplinary Feasible Optimization Solution:**  $[O_1, O_2]$ . Each of the disciplinary optimization problems is solved on a MDA and MDS feasible solutions (see Fig.4):  $[O_1, O_2] \equiv [O_1([A_1, A_2], [S_1, S_2]), O_2([A_1, A_2], [S_1, S_2])]$ . Since zero errors in the states (3.3) and costates (3.5) are assumed, only the system of the design equations (3.4) need to be considered:

$$(4.3) \quad \begin{aligned} I_{b_1} + R_{1,b_1}^* \Lambda_1 + R_{2,b_1}^* \Lambda_2 &= 0 \\ I_{b_2} + R_{1,b_2}^* \Lambda_1 + R_{2,b_2}^* \Lambda_2 &= 0 \end{aligned}$$

where the following notation is used  $I_{b_k} = \frac{\partial I}{\partial b_k}$  and  $R_{i,b_j}^* = \frac{\partial R_i^*}{\partial b_j}$ . In that case the system of error equations for the design variables can be written as follows

$$(4.4) \quad \begin{pmatrix} H_{11} & H_{21} \\ H_{12} & H_{22} \end{pmatrix} \begin{pmatrix} \bar{b}_1 \\ \bar{b}_2 \end{pmatrix} = - \begin{pmatrix} g_1 \\ g_2 \end{pmatrix}$$

where  $g_1$  and  $g_2$  are the residuals when solving Eq.(4.3) (these residuals are equal to the sensitivity gradients) and the matrix  $H$  is the transformation between errors and residuals of the design equations (gradients). The matrices  $H_{ii}$  are dominated by the disciplinary Hessians (assuming feasible state solution, the first order term in a Taylor expansion of the gradient is the Hessian, thus, in the first order approximation, the Hessian relates the errors in each of the disciplinary design variables with the negative gradient of that discipline).

Assuming MDA and MDS feasibility at each optimization step, the GGS iteration is defined as in the MDA case with  $O$  replacing  $R$  and where equation (4.4) replaces (2.3) (the Hessian blocks,  $H_{ij}$ , replace the Jacobian blocks,  $R_{ij}$ ).

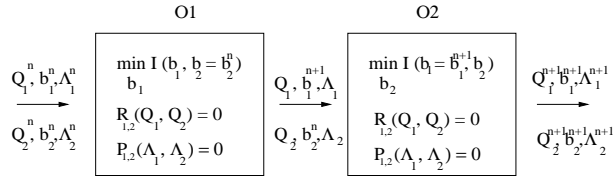


FIG. 4. MD Feasible Optimization Solution:  $[O_1, O_2]$ .

**Lemma 3.1:**

For a two disciplines optimization problem (4.2a-4.2b), starting with errors  $\bar{b}_1$  and  $\bar{b}_2$  in the design variables the MD feasible scheme,  $[O_1, O_2]$ , results in the following expressions for errors reduction:

$$(4.5) \quad \begin{aligned} \bar{b}_1^{n+1} &= \left[ H_{11}^{-1} H_{21} (H_{22}^{n-1})^{-1} H_{12}^{n-1} \right] \bar{b}_2 \\ \bar{b}_2^{n+1} &= \left[ H_{22}^{-1} H_{12} H_{11}^{-1} H_{21} \right] \bar{b}_2. \end{aligned}$$

The proof is similar to the proof of Lemma 1.

The *convergence matrix* in that case is given by

$$(4.6) \quad \mathcal{M}_H = H_{22}^{-1} H_{21} H_{11}^{-1} H_{12},$$

and the convergence factor is bounded by

$$(4.7) \quad \mu_H \leq \rho^{\frac{1}{2}} \left( \mathcal{M}_H^* \mathcal{M}_H \right).$$

**4.2. Single Discipline Feasible Optimization Solution:**  $[O_1(A_1, S_1), O_2(A_2, S_2)]$ . In this section we estimate the convergence factor for the solution in which there is decoupling of the analysis, the sensitivity, and the optimization solutions of one discipline from the other as shown in Fig.5. In terms of the notation we have used so far the decoupled scheme is denoted by  $[O_{k_1}(A_{k_1}, S_{k_1}), O_{k_2}(A_{k_2}, S_{k_2})]$ , i.e., optimizer of system  $k_1$  is using repetitive calls to the analysis and sensitivity analyzers of system  $k_1$  (and uses fixed values of states and sensitivities of system  $k_2$ ) followed by optimizer of system  $k_2$  which acts similarly for system  $k_2$ .

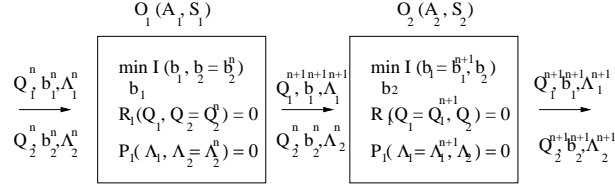


FIG. 5. *Single Discipline Feasible Optimization Solution:  $[O_1(A_1, S_1), O_2(A_2, S_2)]$ .*

The MD scheme under study is summarized by the following two steps scheme. Starting with an initial approximation,  $(Q_1^0, Q_2^0, \Lambda_1^0, \Lambda_2^0, b_1^0, b_2^0)$ , iteration  $n + 1$  (where  $n > 0$ ) is given by:

Scheme 3.2: A GGS MDO Iteration:  $(O_1(A_1, S_1), O_2(A_2, S_2))$

Step 1:  $O_1[A_1, S_1]$ ,

Solve for  $b_1^{n+1}$  the optimization problem  
 $\min_{b_1^{n+1}} I(Q_1^{n+1}, Q_2 = Q_2^n, b_1^{n+1}, b_2 = b_2^n)$   
 subject to  
 $R_1(Q_1^{n+1}, Q_2 = Q_2^n, b_1^{n+1}) = 0.$

Step 2:  $O_2[A_2, S_2]$ ,

Solve for  $b_2^{n+1}$  the optimization problem  
 $\min_{b_2^{n+1}} I(Q_1 = Q_1^{n+1}, Q_2^{n+1}, b_1 = b_1^{n+1}, b_2^{n+1})$   
 subject to  
 $R_2(Q_1 = Q_1^{n+1}, Q_2^{n+1}, b_2^{n+1}) = 0.$

**Lemma 3.2:**

For a two disciplines optimization problem (4.2a-4.2b), starting with errors  $b_1$  and  $b_2$  in the design variables and assuming that the errors in the states satisfy the quasi-linear approximation (2.3), then a single discipline feasible GGS iteration,  $(O_1(A_1, S_1), O_2(A_2, S_2))$ , results in the following errors reduction:

$$\begin{aligned}\bar{e}_1^{n+1} &= \left( O_{11}^{-1} O_{12} (O_{22}^{n-1})^{-1} O_{21}^{n-1} \right) \bar{e}_1 \\ \bar{e}_2^{n+1} &= \left( O_{22}^{-1} O_{21} O_{11}^{-1} O_{12} \right) \bar{e}_2\end{aligned}$$

where the matrices  $O_{ij}$  are defined by

$$(4.8) \quad O_{ij} = \begin{pmatrix} R_{i,Q_j} & 0 & R_{i,b_j} \\ P_{i,Q_j} & P_{i,\Lambda_j} & P_{i,b_j} \\ g_{i,Q_j} & g_{i,\Lambda_j} & g_{i,b_j} \end{pmatrix}$$

and  $\bar{e}_i = (\bar{Q}_i, \bar{\Lambda}_i, \bar{b}_i)$ .

**Proof:**

In terms of the matrices  $O_{ij}$  the relation between the errors and the residuals is given by

$$(4.9) \quad -\begin{pmatrix} r_1 \\ r_2 \end{pmatrix} = \begin{pmatrix} O_{11} & O_{12} \\ O_{21} & O_{22} \end{pmatrix} \begin{pmatrix} \bar{e}_1 \\ \bar{e}_2 \end{pmatrix}.$$

where  $r_i = (R_i, P_i, g_i)$ .

The GGS MDO iteration is updating the variables  $(Q_1, \Lambda_1, b_1)$  and  $(Q_2, \Lambda_2, b_2)$  with the quantities  $\tilde{e}_1$  and  $\tilde{e}_2$  respectively which satisfy the following equation:

$$(4.10) \quad -\begin{pmatrix} r_1 \\ r_2 \end{pmatrix} = \begin{pmatrix} O_{11} & 0 \\ O_{21} & O_{22} \end{pmatrix} \begin{pmatrix} \tilde{e}_1 \\ \tilde{e}_2 \end{pmatrix}.$$

We brought the MDO problem into the same form as the MDA problem (see Eqs. (2.3) and (2.5)) with the changes  $R_{i,Q_j} \rightarrow O_{ij}$ ,  $R_j \rightarrow r_j$ ,  $\bar{Q} \rightarrow \bar{e}$ , and  $\tilde{Q} \rightarrow \tilde{e}$ . Using Lemma 1 we conclude that

$$(4.11) \quad \begin{aligned} \bar{e}_1^{n+1} &= (O_{11}^{-1} O_{12} (O_{22}^{n-1})^{-1} O_{21}^{n-1}) \bar{e}_1 \\ \bar{e}_2^{n+1} &= (O_{22}^{-1} O_{21} O_{11}^{-1} O_{12}) \bar{e}_2. \end{aligned}$$

□

The convergence matrix in this case is given by

$$(4.12) \quad \mathcal{M}_o = O_{22}^{-1} O_{21} O_{11}^{-1} O_{12}.$$

As a result of one iteration  $(O_1(A_1, S_1), O_2(A_2, S_2))$  the total error in the variables of discipline 2 (and also in the transformed variables of discipline 1 (see Sec.2.2.1))  $\vec{e} = (\bar{Q}, \bar{\lambda}, \bar{b})$  is reduced by

$$(4.13) \quad \vec{e}^{n+1} = \mathcal{M}_o \vec{e}.$$

An upper bound for the convergence factor,  $\mu_o$ , is estimated by the following formula:

$$(4.14) \quad \mu_o \leq \rho^{\frac{1}{2}}(\mathcal{M}_o^* \mathcal{M}_o).$$

**5. Test Case I: a Non-Linear Algebraic Example.** In this section we treat a set of two non-linear algebraic equations. The aim here is to demonstrate how the MD convergence estimates are computed when the state equations are non-linear. In this example the estimates will be computed in the same space as the numerical computation is performed, in contrast to the next section in which the estimates are approximated in the infinite dimensional space while the equations are solved in finite dimension. In non-linear problems the equations are first linearized and the convergence theory is applied to approximate the MD convergence rate on the linearized system.

**5.1. Multidisciplinary Analysis.** Let us examine a simple set of non-linear algebraic equations:

$$(5.1) \quad \begin{aligned} x_1^3 + x_2 &= b_1 \\ x_1 + x_2^3 &= b_2 \end{aligned}$$

where we set  $b_1 = b_2 = 2$ . A solution of the above system is given by  $(x_1 = 1, x_2 = 1)$ .

A GGS iteration for the iterative solution of the system (5.1),  $(A_1, A_2)$ , is the Gauss-Seidel (GS) iteration. The convergence matrix (a scalar in this case) for the “MD” iteration  $(A_1, A_2)$  is given by (Eq. (2.13)):

$$(5.2) \quad \mu_a(n > 1) \leq R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} R_{1,Q_2} = \frac{1}{9x_1^2 x_2^2}.$$

In this case the convergence factor depends on the states,  $x_1$  and  $x_2$ . At the solution,  $(x_1 = 1, x_2 = 1)$ , the convergence factor is asymptotically equal to  $\frac{1}{9}$  thus the predicted asymptotic convergence rate for the GS iteration for the solution of Eqs.(5.1) is  $\mu_a = \frac{1}{9}$ .

Application of formula (C.8) for the first iteration results in the following inequality

$$(5.3) \quad \mu_a(n=1) \leq \max \left\{ \frac{1}{3x_1^2} \frac{|\bar{x}_2^0|}{|\bar{x}_1^0|}, \frac{1}{9x_1^2 x_2^2} \right\}.$$

Fig.6 depicts the actual convergence rate versus the theoretical upper bound, where  $\mu_{theory}$  given in (5.2-5.3), and

$$\mu_{actual} = \max \left\{ \frac{|\bar{x}_1^{n+1}|}{|\bar{x}_1^n|}, \frac{|\bar{x}_2^{n+1}|}{|\bar{x}_2^n|} \right\}.$$

For  $n \geq 2$  both  $\mu_{theory}$  and  $\mu_{actual}$  are equal to  $\mu = \frac{1}{9}$ .

**5.2. Multidisciplinary Adjoint.** We define the cost functional

$$(5.4) \quad I(x_1, x_2) = (x_1 x_2 - 1)^2 + \frac{1}{4} x_1^2 + x_2^2,$$

where  $x_1$  and  $x_2$  satisfy Eq.(5.1).

The sensitivities  $\frac{dI}{db_1}$  and  $\frac{dI}{db_2}$  are given by

$$(5.5) \quad \begin{aligned} g_1 &= \frac{dI}{db_1} = -\lambda_1 \\ g_2 &= \frac{dI}{db_2} = -\lambda_2 \end{aligned}$$

where the costates,  $\lambda_1$  and  $\lambda_2$ , satisfy the adjoint equations:

$$(5.6) \quad \begin{aligned} 3x_1^2 \lambda_1 + \lambda_2 &= -I_{x_1} = -\left(2x_2(x_1 x_2 - 1) + \frac{1}{2}x_1\right) \\ \lambda_1 + 3x_2^2 \lambda_2 &= -I_{x_2} = -\left(2x_1(x_1 x_2 - 1) + 2x_2\right). \end{aligned}$$

**5.2.1. Multidisciplinary Feasible Sensitivity Solution:**  $[S_1[A_1, A_2], S_2[A_1, A_2]]$ . Since all the operators in this case  $R_{i,Q_j}$  are real scalars the convergence estimates are identical to the MDA case. In the numerical test the MDA problem is solved first and then the GS scheme is applied to the adjoint system (5.6). Fig.7a depicts the actual versus the upper bound convergence rate for this scheme. As in the MDA case there is a good agreement between the theoretical upper bound and the actual convergence rates.

**5.2.2. Single Discipline Feasible Sensitivity Solution:**  $[S_1(A_1), S_2(A_2)]$ . We apply Lemma 2.2 to estimate the upper bound for the convergence rate. In this case the matrices  $S_{ij}$  are given by

$$(5.7a) \quad S_{11} = \begin{pmatrix} 3x_1^2 & 0 \\ 6x_1 \lambda_1 + I_{x_1, x_1} & 3x_1^2 \end{pmatrix} \quad ; \quad S_{12} = \begin{pmatrix} 1 & 0 \\ I_{x_1, x_2} & 1 \end{pmatrix}$$

$$(5.7b) \quad S_{21} = \begin{pmatrix} 1 & 0 \\ I_{x_2, x_1} & 1 \end{pmatrix} \quad ; \quad S_{22} = \begin{pmatrix} 3x_2^2 & 0 \\ 6x_2 \lambda_2 + I_{x_2, x_2} & 3x_2^2 \end{pmatrix}$$

where

$$(5.8) \quad \begin{aligned} I_{x_1, x_1} &= 2x_2 x_2 + \frac{1}{2} \\ I_{x_1, x_2} &= 4x_1 x_2 - 2 \\ I_{x_2, x_1} &= 4x_1 x_2 - 2 \\ I_{x_2, x_2} &= 2x_1 x_1 + 2. \end{aligned}$$



The upper bound for the convergence rate is estimated by

$$\mu_s \leq \|S_{22}^{-1} S_{21} S_{11}^{-1} S_{12}\|.$$

In the numerical test scheme 2.2 was applied  $[S_1(A_1), S_2(A_1)]$ . Fig.7b depicts the actual versus theoretical upper bound of the convergence for this case. The theoretical upper bound for the first GGS iteration is  $\mu_{theory}(n=1) \approx 2.6$  ( $n=1$  in the figure). The actual convergence rate approaches the MDA convergence rate  $\mu_a = \frac{1}{9}$  for  $n \gg 1$ .

**5.3. Multidisciplinary Optimization.** The optimization problem is defined by

$$(5.9) \quad \min_{b_1, b_2} I(x_1, x_2)$$

subject to Eq.(5.1), where the cost functional  $I(x_1, x_2)$  is defined in (5.4).

**5.3.1. Multidisciplinary Feasible Optimization Solution:**  $[O_1, O_2]$ . The Hessian is computed with a combination of the adjoint and direct-differentiation method (the combination of the adjoint and sensitivity methods to compute the Hessian was originally introduced by R. Haftka [13]). The Hessian is given by

$$(5.10) \quad H = \frac{\partial g}{\partial b} + \frac{\partial g}{\partial Q} \frac{\partial Q}{\partial b} + \frac{\partial g}{\partial \lambda} \lambda'$$

where  $\lambda' = \frac{\partial \lambda}{\partial b}$  satisfies

$$(5.11) \quad \frac{\partial P}{\partial b} + \frac{\partial P}{\partial Q} \frac{\partial Q}{\partial b} + \frac{\partial P}{\partial \lambda} \lambda' = 0$$

and  $P = P(Q, \lambda, b)$  denotes the residuals of the costate equation

$$(5.12) \quad P = \left( \frac{\partial R}{\partial Q} \right)^* \lambda + \left( \frac{\partial I}{\partial Q} \right)^*.$$

For the problem (5.9)

$$(5.13) \quad \frac{\partial g}{\partial b} = \frac{\partial g}{\partial Q} = \frac{\partial P}{\partial b} = 0 \quad \text{and} \quad \frac{\partial g}{\partial \lambda} = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}.$$

Thus the Hessian is given by

$$(5.14) \quad \begin{pmatrix} H_{11} & H_{21} \\ H_{12} & H_{22} \end{pmatrix} = \lambda' = - \left( \frac{\partial P}{\partial \lambda} \right)^{-1} \frac{\partial P}{\partial Q} \frac{\partial Q}{\partial b} =$$

$$= - \begin{pmatrix} 3x_1^2 & 1 \\ 1 & 3x_2^2 \end{pmatrix}^{-1} \begin{pmatrix} 6x_1\lambda_1 + I_{x_1, x_1} & I_{x_1, x_2} \\ I_{x_2, x_1} & 6x_2\lambda_2 + I_{x_2, x_2} \end{pmatrix} \begin{pmatrix} 3x_1^2 & 1 \\ 1 & 3x_2^2 \end{pmatrix}^{-1}$$

where  $I_{x_i, x_j}$  are given in (5.8)

The convergence factor  $\mu_H$  for this scheme is estimated by

$$(5.15) \quad \mu_H \leq \rho^{\frac{1}{2}}(\mathcal{M}_H^* \mathcal{M}_H)$$

where  $\mathcal{M}_H$  is given by

$$(5.16) \quad \mathcal{M}_H = H_{22}^{-1} H_{21} H_{11}^{-1} H_{12}.$$

In the numerical test each of the sub-optimization problems was solved at a time, i.e.,

$$O_1 = \min_{b_1} I(x_1) \quad ; \quad O_2 = \min_{b_2} I(x_2),$$

where full MDA and MDS feasibility were maintained at each solution. Fig. 8a depicts the actual versus theoretical upper bound of the convergence for this case. The actual and theoretical upper bound convergence factors for the first GGS iteration are given by  $\mu_{actual}(n=1) \approx 2.7$  and  $\mu_{theory}(n=1) \approx 9.5$  respectively. The asymptotic convergence rates are given by  $\mu_{actual}(n=1) \approx 0.93$  and  $\mu_{theory}(n=1) \approx 0.95$ .

**5.4. Single Discipline Feasible Optimization Solution:**  $[O_1(A_1, S_1), O_2(A_2, S_2)]$ . The convergence of the GGS scheme,  $[O_1(A_1, S_1), O_2(A_2, S_2)]$ , is determined by the matrices  $O_{ij}$  defined in Eq.(4.8). For the problem (5.9) the matrices  $O_{ij}$  are given in the following:

$$(5.17a) \quad O_{11} = \begin{pmatrix} R_{1,Q_1} & 0 & R_{1,b_1} \\ P_{1,Q_1} & P_{1,\lambda_1} & P_{1,b_1} \\ g_{1,Q_1} & g_{1,\lambda_1} & g_{1,b_1} \end{pmatrix} = \begin{pmatrix} 3x_1^2 & 0 & -1 \\ 6x_1\lambda_1 + I_{x_1,x_1} & 3x_1^2 & 0 \\ 0 & -1 & 0 \end{pmatrix}$$

$$(5.17b) \quad O_{12} = \begin{pmatrix} R_{1,Q_2} & 0 & R_{1,b_2} \\ P_{1,Q_2} & P_{1,\lambda_2} & P_{1,b_2} \\ g_{1,Q_2} & g_{1,\lambda_2} & g_{1,b_2} \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ I_{x_1,x_2} & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$(5.17c) \quad O_{21} = \begin{pmatrix} R_{2,Q_1} & 0 & R_{2,b_1} \\ P_{2,Q_1} & P_{2,\lambda_1} & P_{2,b_1} \\ g_{2,Q_1} & g_{2,\lambda_1} & g_{2,b_1} \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ I_{x_2,x_1} & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$(5.17d) \quad O_{22} = \begin{pmatrix} R_{2,Q_2} & 0 & R_{2,b_2} \\ P_{2,Q_2} & P_{2,\lambda_2} & P_{2,b_2} \\ g_{2,Q_2} & g_{2,\lambda_2} & g_{2,b_2} \end{pmatrix} = \begin{pmatrix} 3x_2^2 & 0 & -1 \\ 6x_2\lambda_2 + I_{x_2,x_2} & 3x_2^2 & 0 \\ 0 & -1 & 0 \end{pmatrix}.$$

An upper bound for the convergence factor is estimated by the spectral radius of  $\mathcal{M}_O^* \mathcal{M}_O$ , where  $\mathcal{M}_O = O_{22}^{-1} O_{21} O_{11}^{-1} O_{12}$ :

$$\mu_o \leq \rho^{\frac{1}{2}}(\mathcal{M}_O^* \mathcal{M}_O).$$

Fig.8b depicts the actual versus theoretical upper bound of the convergence for this case. The actual and theoretical upper bound convergence factors for the first GGS iteration are given by  $\mu_{actual}(n=1) \approx 1.9$  and  $\mu_{theory}(n=1) \approx 4.3$  respectively. In the numerical test the solution of the problem was obtained after the third iteration in which the error was reduced by a factor of approximately  $1.75 \cdot 10^{-6}$  (the optimal solution is given by  $x_1 = 1, x_2 = \frac{1}{2}, b_1 = 1\frac{1}{2}$ , and  $b_2 = 1\frac{1}{8}$ ). It is interesting to note that in this case the solution required much less optimization steps than in the previous case where full feasibility was maintained. This was predicted by the analysis although the upper bound for the convergence is higher than the one found in practice: for  $n > 1$ ,  $\mu_{theory} \approx 0.25$ .

**6. Test Case II: A Coupled System of PDEs Modeling Static Aeroelasticity.** In this section we treat a set of two coupled PDEs with the aim to demonstrate how estimates in the PDE level can be used to approximate the different convergence factors in the problem. Since the actual numerical computation is done in a finite dimensional space, the continuum estimates holds only in the limit of the discrete mesh-size,  $h$ , approaching zero. Nevertheless, the continuum estimates give a good approximation of the actual discrete convergence (as long as the discrete mesh is not too coarse). The coupling estimates can be derived also in the discrete level where the different Jacobians are large matrices (rather than operators).

In this example we use Fourier analysis and Parseval's relation to estimate the norms of the convergence operators involved, however it is not necessarily the only way to get such estimates. The problem under consideration is linear in the state variables with non-constant coefficients. However, the optimization problem is non-linear since the design variables multiply the states. In the general case where the state equations are non-linear the first step in the analysis is to linearize them resulting in a linear equation with non-constant coefficients similar to the problem under consideration in this section.

This problem contains some of the physical features of static aeroelasticity. Aeroelastic optimization is a major MDO problem in aerospace industry (e.g., [14] and references therein). The aerodynamic state equation models the flow around a body and the design variables are some parameters defining the shape of that body. The aerodynamic cost functional is typically the drag or some measure of the closeness to some specified pressure distribution. The structure state equation typically results from a finite element analysis of the structure and the design variables are some parameters which determine the stiffness of the structure. The structure cost functional is typically the weight and there are constraints on the stress on different elements in the structure. There is not a unique way to define an MDO problem in that field and hence we will assume a simple model problem that contains some of the physics of the real problem.

**6.1. Problem Definition.** We consider a two dimensional potential flow over a one dimensional beam. The MDO problem is to compute the set of rigidity parameters,  $\{D_i^h\}_{i=1}^N$ , and the set of shape parameters,  $\{\alpha_i^h\}_{i=1}^N$ , such that the following cost functional is minimized (we denote the discrete quantities by a superscript  $h$ ),

$$(6.1) \quad F^h(\phi^h, W^h, \alpha^h, D^h) = \sum_{i=1}^N \left[ \gamma_1 \left( \partial_x \phi_i^h - f_i^{*h} \right)^2 + \gamma_2 (D_i^h)^{\frac{1}{2}} + \gamma_3 (\partial_x \phi_i^h) W_i^h + \gamma_4 \frac{1}{2} (\alpha_i^h)^2 \right]$$

subject to the inequality constraint

$$(6.2) \quad D_i^h \geq D_{min} \quad 1 < i < N$$

and to the following finite difference equations,

$$(6.3) \quad \begin{aligned} (1 - M_\infty^2) \partial_{xx}^h \phi_{i,k}^h + \partial_{zz}^h \phi_{i,k}^h &= 0 & 1 < i, k < N \\ \partial_z^h \phi_{i,1}^h &= \partial_x^h (\alpha_i^h + W_i^h) & 1 < i < N \\ \phi_{1,k}^h &= \phi_{2,k}^h & 1 < k < N \\ \phi_{N,k}^h &= \phi_{N-1,k}^h & 1 < k < N \\ \phi_{i,N}^h &= 0 & 1 < i < N \end{aligned}$$

$$(6.4) \quad \begin{aligned} \partial_{xx}^h (D_i^h \partial_{xx}^h W_i^h) &= -p_i^h \left( (\phi_x^h)_i \right) & 1 < i < N \\ W_1^h &= W_N^h = 0 \\ \partial_{xx}^h W_1^h &= \partial_{xx}^h W_N^h = 0 & \text{for a simply supported beam} \end{aligned}$$

where  $\partial_x^h, \partial_z^h, \partial_{xx}^h$  and  $\partial_{zz}^h$  denote finite difference operators for the first and second derivatives in the  $x$  and  $z$  directions respectively.

The pressure,  $p$ , depends on the potential by the Bernoulli law (we assume  $\partial_x \phi \ll U_\infty$ ):

$$(6.5) \quad p = p_\infty + \rho_\infty U_\infty^2 \partial_x \phi.$$

In the numerical test the far field parameters were set to unity except the far field Mach number which was set to zero (the latter was chosen to simplify the analytical estimate of the coupling):

$$p_\infty = \rho_\infty = U_\infty = 1 \quad ; \quad M_\infty = 0.$$

The forth term in the cost functional was added for uniqueness of the optimal solution  $\alpha^*$  (since only the derivative  $\partial_x \alpha$  appears in the equations). The weights in the cost functional were determined to establish a significant coupling between the disciplines, i.e., at the optimal solution the deflection,  $W^*$ , and the shape,  $\alpha^*$ , have the same order of magnitude:

$$\gamma_1 = 1 \quad ; \quad \gamma_2 = 0.01 \quad ; \quad \gamma_3 = -1 \quad ; \quad \gamma_4 = 1.$$

In order to avoid singularities in the beam equation,  $D^h = 0$ , an inequality constraint has been applied on the rigidity:

$$(6.6) \quad D(x) \geq D_{min}(x) \quad 0 \leq x \leq 1$$

where the minimal value of the rigidity was set to  $D_{min}(x) = 10^{-4}$ .

The computational grid consisted of an  $(N \times N)$  grid on which the potential equation was solved in the whole domain while the beam equation was solved on the boundary ( $z = 0$ ). On each grid point on the boundary,  $1 \leq i \leq N$ , two design variables were defined:  $\alpha_i^h$  and  $D_i^h$ .

**6.2. MDA.** The MDA problem is to solve the system of discretized PDEs (6.3-6.4) for  $\phi^h$  and  $W^h$  where the design parameters,  $\alpha^h$  and  $D^h$ , are fixed. A GGS iteration is composed of two steps; solving Eq.(6.3) for  $\phi^h$  keeping  $W^h$  fixed, followed by the solution of Eq.(6.4) for  $W^h$  keeping  $\phi^h$  fixed. By Eq.(2.13) the convergence of the above GGS iteration is determined by the norm of the *convergence matrix*,  $\mathcal{M}_a = R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} R_{1,Q_2}$ . In the following Fourier analysis in the continuum level is used to estimate the norm of  $\mathcal{M}_a$ . Since the estimate is derived in the continuum level and the numerical test is done in the discrete level, the derived estimate is only an approximation (that is expected to be more accurate with the refinement of the discretization).

#### An Estimate of the convergence factor using Parseval's Relation

We now make use of Parseval's relation to estimate the norm of the convergence matrix,  $\mathcal{M}_a$ , in the PDE level. Parseval's relation states that the  $L^2$  norm of the error in real space is equal to the  $L^2$  norm of the error in Fourier space:

$$(6.7) \quad \|\vec{e}\|_{L^2} = \|\hat{\vec{e}}_k\|_{L^2}.$$

By Eq.(2.13)

$$(6.8) \quad \vec{e}_2^{n+1} = \mathcal{M}_a \vec{e}_2$$

and therefore (see Appendix A)

$$(6.9) \quad \|\bar{e}_2^{n+1}\| \leq \max_k \left( \hat{\mathcal{M}}_a^* \hat{\mathcal{M}}_a \right)^{\frac{1}{2}} \|\bar{e}_2\|.$$

An upper bound for the convergence factor,  $\mu_a$ , is estimated with

$$(6.10) \quad \mu_a \leq \max_k \left( \hat{\mathcal{M}}_a^* \hat{\mathcal{M}}_a \right)^{\frac{1}{2}} = \max_k \left( \frac{(2k\pi)^2}{\hat{G}_W^*(D) \hat{G}_W(D)} \right)^{\frac{1}{2}}.$$

**6.2.1. Numerical Results.** In the numerical test the scheme  $[A_1, A_2]$  was applied. A random number generator was used to give the initial values to the state variables,  $\phi^h$  and  $W^h$ . At each iteration the single discipline analysis problem (the the potential equation for  $\phi^h$ ) was solved to machine zero accuracy, keeping the other discipline state variables ( $W^h$ ) fixed. This was followed by solving the second discipline analysis problem (Beam equation for  $W^h$ ) while keeping the updated values of the first discipline ( $\phi^h$ ) fixed. The equations were solved with a second order accurate finite difference iterative method.

Fig.9 depicts the actual convergence rate versus the theoretical upper bound, where  $\mu_{theory}$  given in (6.10) and

$$\mu_{actual} = \max \left\{ \frac{\|\bar{\phi}^{n+1}\|}{\|\bar{\phi}^n\|}, \frac{\|\bar{W}^{n+1}\|}{\|\bar{W}^n\|} \right\}.$$

Since  $\hat{G}_W(D)$  in (6.10) depends on the values of the rigidity,  $\{D_i^h\}_{i=1}^N$ , the estimate (6.10) was computed by the analysis code for the actual values of the rigidity at each iteration. An alternative could have been a good a-priori estimate of the minimum value of  $\hat{G}_W(D)$ . The results show good agreement with the predictions of the convergence estimates. It is interesting to note that although the estimate for the convergence factor depends on the non-constant coefficient  $D^h$  still the predicted values of  $\mu_a$  are fixed (for  $n > 1$ ) on the value  $\mu_{theory} \approx 7 \times 10^{-3}$ , possibly due to the determination of the extremal values of  $D^h$ ,  $\partial_x D^h$  and  $\partial_{xx} D^h$  during the early stage of the computation. The actual convergence rate is about  $\mu_{actual} \approx 1 - 3 \times 10^{-3}$ , (lower than the upper bound estimate). After the fourth iteration the errors in the state variables reach the level of machine accuracy and the computation is terminated.

**6.3. MDS.** In the MDS problem the sensitivities on the cost functional, (6.1), are computed with respect to the design variables  $D^h$  and  $\alpha^h$ . We choose to use the adjoint method (see appendix B) to compute these sensitivities since it is the most efficient method if there are less “outputs” (in this case the only output is the cost functional) than “inputs” ( $2N$  design variables) in the problem.

The costate equations for that problem, in the continuum level, are given by (the costate flow and structure variable are denoted by  $\Lambda_1 = \lambda$  and  $\Lambda_2 = \eta$  respectively):

#### Flow Costate Equation

$$(6.11) \quad \begin{aligned} \Delta \lambda &= 0 & \text{in } \Omega &= \{0 < x < 1 ; 0 < y < 1\} \\ \partial_z \lambda &= \partial_x \eta + 2\gamma_1(\partial_{xx} \phi - \partial_x f^*) + \gamma_3 \partial_x W & \text{on } z &= 0 \\ \partial_x \lambda &= 0 & \text{on } x &= 0 \\ \partial_x \lambda &= 0 & \text{on } x &= 1 \\ \lambda &= 0 & \text{on } z &= 1. \end{aligned}$$

### Structure Costate Equation

$$\begin{aligned}
(6.12) \quad & \partial_{xx}(D\partial_{xx}\eta) = -\partial_x\lambda - \gamma_3\partial_x\phi && \text{on } z = 0 ; 0 < x < 1 \\
& \eta(0) = \eta(1) = 0 \\
& \partial_{xx}\eta(0) = \partial_{xx}\eta(1) = 0 && \text{for a simply supported beam .}
\end{aligned}$$

Having defined the states and costates, the sensitivity gradients,  $g_1 = \frac{dF}{d\alpha}$  and  $g_2 = \frac{dF}{dD}$ , are given by

$$\begin{aligned}
(6.13) \quad & g_1 = \partial_x\lambda + \gamma_4\alpha && \text{on } z = 0 ; 0 < x < 1. \\
& g_2 = \partial_{xx}\eta\partial_{xx}W + \frac{\gamma_2}{2}D^{-\frac{1}{2}}
\end{aligned}$$

The MDS problem, for this example, is to solve Eqs.(6.11-6.12) for  $\lambda$  and  $\eta$ . We apply two schemes: the MD feasible sensitivity solution  $[S_1, S_2]$  and the single discipline sensitivity solution  $[S_1(A_1), S_2(A_2)]$  requiring only single discipline state feasibility at each step (see Secs.3.2-3.3).

### Multidisciplinary Feasible Sensitivity Solution: $[S_1, S_2]$

By Lemma 2.1 (Eq.(3.8)) the convergence matrix for the MD feasible sensitivity scheme is given by

$$(6.14) \quad \mathcal{M}_{a^*} = R_{2,Q_2}^{-*} R_{2,Q_1}^* R_{1,Q_1}^{-*} R_{1,Q_2}^* = \frac{2k\pi}{\hat{G}_W^*(D)} = \mathcal{M}_a^*.$$

We conclude that

$$(6.15) \quad \|\mathcal{M}_{a^*}\| = \|\mathcal{M}_a\|,$$

thus we predict the same convergence factor as in the MDA case.

### Single Discipline Feasible Sensitivity Solution: $[S_1(A_1), S_2(A_2)]$

The symbol of the convergence matrix for that scheme is given by (see Eq.(3.14))

$$\hat{\mathcal{M}}_s = \hat{S}_{22}^{-1} \hat{S}_{21} \hat{S}_{11}^{-1} \hat{S}_{12} = \begin{pmatrix} \hat{\mathcal{M}}_a & 0 \\ \hat{\mathcal{M}}_{as} & \hat{\mathcal{M}}_{a^*} \end{pmatrix}$$

where

$$(6.16) \quad \hat{\mathcal{M}}_a = \left(\hat{\mathcal{M}}_{a^*}\right)^* = \frac{2k\pi}{\hat{G}_W(D)} \quad ; \quad \hat{\mathcal{M}}_{as} = \frac{4k\pi(\gamma_3 - \gamma_1 2k\pi)}{\hat{G}_W(D)}.$$

An upper bound for the convergence rate is estimated by

$$(6.17) \quad \mu_s \leq \max_k \rho^{\frac{1}{2}} \left( \hat{\mathcal{M}}_s^*(k) \hat{\mathcal{M}}_s(k) \right).$$

**6.3.1. Numerical Results.** In the numerical test the two schemes  $[S_1, S_2]$  and  $[S_1(A_1), S_2(A_2)]$  were tested.

### Multidisciplinary Feasible Sensitivity Solution: $[S_1, S_2]$

In the numerical test the MDA problem was solved first and then the GGS scheme was applied to the adjoint system (6.11-6.12). A random number generator was used to give the initial values to the costate variables:  $\lambda^h$  and  $\eta^h$ . The same procedure as in the MDA case was repeated for the adjoint equations. The theoretical upper bound in this case is identical to the one in the MDA problem (Eq. 6.15). Fig.10a

depicts the actual versus the upper bound convergence rate for this scheme. For iteration number  $n > 1$  the theoretical upper bound settles on  $\mu_{theory} \approx 8 \times 10^{-3}$  while the actual convergence rate for  $n > 1$  is  $\mu_{actual} \approx 2 - 4 \times 10^{-3}$ .

#### Single Discipline Feasible Sensitivity Solution: $[S_1(A_1), S_2(A_2)]$

In this case a random number generator was used to give the initial values to both the state and costate variables:  $\phi^h$ ,  $W^h$ ,  $\lambda^h$  and  $\eta^h$ . At each iteration the single discipline analysis and adjoint problems were solved sequentially (the analysis problem is independent of the adjoint problem).

Fig.10b depicts the actual convergence rate versus the theoretical upper bound, where  $\mu_{theory}$  given in (6.17) and

$$\mu_{actual} = \max \left\{ \frac{\|\bar{\phi}^{n+1} + \bar{\lambda}^{n+1}\|}{\|\bar{\phi}^n + \bar{\lambda}^n\|}, \frac{\|\bar{W}^{n+1} + \bar{\eta}^{n+1}\|}{\|\bar{W}^n + \bar{\eta}^n\|} \right\}.$$

For iteration number  $n > 1$  the theoretical upper bound, computed by (6.17), settles on  $\mu_{theory} \approx 1.1 \times 10^{-2}$  while the actual convergence rate for  $n > 1$  is  $\mu_{actual} \approx 1 - 5 \times 10^{-3}$ .

**6.4. MDO.** The MDO problem is to solve the optimization problem (6.1-6.4). The MDO problem is divided into two sub-optimization problems:  $O_1$  and  $O_2$ . In  $O_1$  the design variable is  $\alpha^h$  while  $D^h$  is fixed and in  $O_2$  it is visa versa. In the numerical test two schemes were applied: the MD feasible scheme,  $[O_1, O_2]$ , and the single discipline feasible scheme,  $[O_1(A_1, S_1), O_2(A_2, S_2)]$ .

**6.4.1. Fourier Analysis for the MD Feasible Scheme  $[O_1, O_2]$ .** By Eq.(4.6) the *convergence matrix* in this case is given by

$$(6.18) \quad \mathcal{M}_H = H_{22}^{-1} H_{21} H_{11}^{-1} H_{12}.$$

Following [10] the symbol of the Hessian for this problem is computed by the following procedure. The map, in Fourier space, between the errors in the design variables and the state variables is computed:

$$(6.19a) \quad \begin{pmatrix} \hat{\phi}(k) \\ \hat{W}(k) \end{pmatrix} = - \begin{pmatrix} 2\pi k & -2\pi i k \\ 2\pi i k & \hat{G}_W(D) \end{pmatrix}^{-1} \begin{pmatrix} -2\pi i k & 0 \\ 0 & \hat{G}_D(W) \end{pmatrix} \begin{pmatrix} \hat{\alpha}(k) \\ \hat{D}(k) \end{pmatrix}$$

The solution of (6.19a) is substituted in the following equation for the map, in Fourier space, between the errors in the design variables and the costate variables:

$$(6.19b) \quad \begin{pmatrix} \hat{\lambda}(k) \\ \hat{\eta}(k) \end{pmatrix} = - \begin{pmatrix} 2\pi k & -2\pi i k \\ 2\pi i k & \hat{G}_W(D) \end{pmatrix}^{-1} \begin{pmatrix} 2\gamma_1(2\pi k)^2 & -\gamma_3(2\pi i k) \\ \gamma_3(2\pi i k) & 0 \end{pmatrix} \begin{pmatrix} \hat{\phi}(k) \\ \hat{W}(k) \end{pmatrix} \\ - \begin{pmatrix} 2\pi k & 2\pi i k \\ 2\pi i k & \hat{G}_W(D) \end{pmatrix}^{-1} \begin{pmatrix} 0 & 0 \\ 0 & \hat{G}_D(\eta) \end{pmatrix} \begin{pmatrix} \hat{\alpha}(k) \\ \hat{D}(k) \end{pmatrix}.$$

Finally, both the solutions of (6.19a) and of (6.19b) are substituted in the expression for the symbols of the sensitivity gradients to compute the map, in Fourier space, between the errors in the design variables and the residuals of the design equations (the gradients):

$$\begin{aligned}
\begin{pmatrix} \hat{g}_1(k) \\ \hat{g}_2(k) \end{pmatrix} &= \begin{pmatrix} 0 & 0 \\ 0 & \hat{G}_D(\eta) \end{pmatrix} \begin{pmatrix} \hat{\phi}(k) \\ \hat{W}(k) \end{pmatrix} + \begin{pmatrix} 2\pi i k & 0 \\ 0 & \hat{G}_D(W) \end{pmatrix} \begin{pmatrix} \hat{\lambda}(k) \\ \hat{\eta}(k) \end{pmatrix} \\
(6.19c) \quad &+ \begin{pmatrix} \gamma_4 & 0 \\ 0 & -\gamma_2 \frac{1}{4} D^{-\frac{3}{2}} \end{pmatrix} \begin{pmatrix} \hat{\alpha}(k) \\ \hat{D}(k) \end{pmatrix}.
\end{aligned}$$

As discussed in [10] the symbol of that map is the symbol of the MD Hessian:

$$(6.20) \quad \begin{pmatrix} \hat{g}_1(k) \\ \hat{g}_2(k) \end{pmatrix} = - \begin{pmatrix} \hat{H}_{11}(k) & \hat{H}_{12}(k) \\ \hat{H}_{21}(k) & \hat{H}_{22}(k) \end{pmatrix} \begin{pmatrix} \hat{\alpha}(k) \\ \hat{D}(k) \end{pmatrix}.$$

Having computed the symbol of the convergence matrix for that problem,

$$\hat{\mathcal{M}}_H(k) = \hat{H}_{22}^{-1}(k) \hat{H}_{21}(k) \hat{H}_{11}^{-1}(k) \hat{H}_{12}(k),$$

an upper bound for the convergence rate is estimated by

$$(6.21) \quad \mu_H \leq \max_k \rho^{\frac{1}{2}} \left( \hat{\mathcal{M}}_H^*(k) \hat{\mathcal{M}}_H(k) \right).$$

**6.4.2. Fourier Analysis for the SD Feasible Scheme**  $[O_1(A_1, S_1), O_2(A_2, S_2)]$ . By Lemma 3.2 the *convergence matrix* in this case is given by

$$(6.22) \quad \mathcal{M}_o = O_{22}^{-1} O_{21} O_{11}^{-1} O_{12}$$

where the operators  $O_{ij}$  are defined in (4.8).

The matrices  $\hat{O}_{ij}$  are given in the following:

$$(6.23a) \quad \hat{O}_{11} = \begin{pmatrix} \hat{R}_{1,Q_1} & 0 & \hat{R}_{1,b_1} \\ \hat{P}_{1,Q_1} & \hat{P}_{1,\lambda_1} & \hat{P}_{1,b_1} \\ \hat{g}_{1,Q_1} & \hat{g}_{1,\lambda_1} & \hat{g}_{1,b_1} \end{pmatrix} = \begin{pmatrix} 2\pi k & 0 & -2\pi i k \\ 2\gamma_1(2\pi k)^2 & 2\pi k & 0 \\ 0 & 2\pi i k & \gamma_4 \end{pmatrix}$$

$$(6.23b) \quad \hat{O}_{12} = \begin{pmatrix} \hat{R}_{1,Q_2} & 0 & \hat{R}_{1,b_2} \\ \hat{P}_{1,Q_2} & \hat{P}_{1,\lambda_2} & \hat{P}_{1,b_2} \\ \hat{g}_{1,Q_2} & \hat{g}_{1,\lambda_2} & \hat{g}_{1,b_2} \end{pmatrix} = \begin{pmatrix} -2\pi i k & 0 & 0 \\ -\gamma_3(2\pi i k) & -2\pi i k & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$(6.23c) \quad \hat{O}_{21} = \begin{pmatrix} \hat{R}_{2,Q_1} & 0 & \hat{R}_{2,b_1} \\ \hat{P}_{2,Q_1} & \hat{P}_{2,\lambda_1} & \hat{P}_{2,b_1} \\ \hat{g}_{2,Q_1} & \hat{g}_{2,\lambda_1} & \hat{g}_{2,b_1} \end{pmatrix} = \begin{pmatrix} 2\pi i k & 0 & 0 \\ \gamma_3(2\pi i k) & 2\pi i k & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$(6.23d) \quad \hat{O}_{22} = \begin{pmatrix} \hat{R}_{2,Q_2} & 0 & \hat{R}_{2,b_2} \\ \hat{P}_{2,Q_2} & \hat{P}_{2,\lambda_2} & \hat{P}_{2,b_2} \\ \hat{g}_{2,Q_2} & \hat{g}_{2,\lambda_2} & \hat{g}_{2,b_2} \end{pmatrix} = \begin{pmatrix} \hat{G}_W(D) & 0 & \hat{G}_D(W) \\ 0 & \hat{G}_W(D) & \hat{G}_D(\eta) \\ \hat{G}_D(\eta) & \hat{G}_D(W) & -\gamma_2 \frac{1}{4} D^{-\frac{3}{2}} \end{pmatrix}.$$

Using Parseval's relation an upper bound for the convergence factor is estimated by the maximal singular value of  $\hat{\mathcal{M}}_O$ , or equivalently by

$$(6.24) \quad \mu_o \leq \max_k \rho^{\frac{1}{2}} (\hat{\mathcal{M}}_O^*(k) \hat{\mathcal{M}}_O(k)),$$

where  $\hat{\mathcal{M}}_O = \hat{O}_{22}^{-1} \hat{O}_{21} \hat{O}_{11}^{-1} \hat{O}_{12}$ .



**6.4.3. Numerical Results.** In the numerical test the two schemes  $[O_1, O_2]$  and  $[O_1(A_1, S_1), O_2(A_2, S_2)]$  were tested.

Multidisciplinary Feasible Optimization Solution:  $[O_1, O_2]$

In the numerical test the MDA and MDS problems were solved to machine zero accuracy at each optimization step. The theoretical upper bound for the convergence rate was computed by (6.21), and the actual rate by

$$\mu_{actual} = \max \left\{ \frac{\|\bar{\alpha}^{n+1}\|}{\|\bar{\alpha}^n\|}, \frac{\|\bar{D}^{n+1}\|}{\|\bar{D}^n\|} \right\}.$$

In that case the error in  $\alpha^h$  reduced at the first iteration by a factor of  $1.3 \times 10^{-5}$  while that of  $D^h$  by  $3.7 \times 10^{-6}$ . Since the error reduction is so significant the computation is terminated after two iterations due to the low numbers involved in the computation at this stage. The theoretical upper bound is  $\mu_{theory} \approx 3.5 \times 10^{-2}$  which is much higher than the actual convergence rate.

Single Discipline Feasible Optimization Solution:  $[O_1(A_1, S_1), O_2(A_2, S_2)]$

In this case at each iteration the single discipline optimization problem was solved while keeping the variables of the other discipline fixed.

Fig.11 depicts the actual convergence rate versus the theoretical upper bound, where  $\mu_{theory}$  given in (6.24) and

$$\mu_{actual} = \max \left\{ \frac{\|\bar{\phi}^{n+1} + \bar{\lambda}^{n+1} + \bar{\alpha}^{n+1}\|}{\|\bar{\phi}^n + \bar{\lambda}^n + \bar{\alpha}^n\|}, \frac{\|\bar{W}^{n+1} + \bar{\eta}^{n+1} + \bar{D}^{n+1}\|}{\|\bar{W}^n + \bar{\eta}^n + \bar{D}^n\|} \right\}.$$

In this case the actual convergence rate for iterations 2,3,4, and 5 are given by  $5.5 \times 10^{-4}$ ,  $1.84 \times 10^{-3}$ ,  $8.8 \times 10^{-4}$ , and  $1.02 \times 10^{-2}$ . The theoretical upper bound is  $\mu_{theory} \approx 5.2 \times 10^{-2}$ . As discussed in [10] the fast convergence of sequential algorithms applied to the aeroelastic model problem indicates of weak coupling between the two disciplines.

**7. Discussion and Concluding Remarks.** We present a quantitative analysis to determine the convergence rate of loosely coupled schemes for solving MD systems of equations.

The sequential scheme, where the problems are solved in the disciplinary level “one-at-a-time”, is identified as a generalization of the Gauss-Seidel (GGS) iterative method. The parallel version of the sequential scheme, where the problems are solved in the disciplinary level in parallel exchanging coupling data after each MD iteration, is identified as a generalization of the Jacobi (GJ) iterative method. Other iterative schemes can be generalized to MD systems (e.g., Richardson, Kaczmarz, Etc.).

The asymptotic convergence rate for the GGS scheme can serve a measure for the coupling between the disciplinary problems since the looser the coupling is the lower is the value of that convergence rate. An upper bound for the convergence rate (convergence factor) is estimated for the multidisciplinary analysis (MDA), sensitivity (MDS), and optimization (MDO) problems.

Five different basic schemes are considered (given here for problems composed of two disciplinary sub-problems). In all the schemes the convergence matrix is given in the general form  $\mathcal{M} = Z_{22}^{-1} Z_{21} Z_{11}^{-1} Z_{12}$ . The

quantities  $Z_{ij}$  depend on the scheme under consideration and are summarized here for the different schemes presented in the paper:

- Sequential GGS scheme for the MDA problem,  $[A_1, A_2]$ :  $Z_{ij} = R_{i,Q_j}$
- Sequential GGS scheme for the MDS problem
  - MD feasible sensitivity solution,  $[S_1, S_2]$ :  $Z_{i,j} = R_{j,Q_i}^*$
  - Single discipline feasible sensitivity solution,  $[S_1(A_1), S_2(A_2)]$ :

$$Z_{i,j} = \begin{pmatrix} R_{i,Q_j} & 0 \\ P_{i,Q_j} & P_{i,\Lambda_j} \end{pmatrix}$$

- Sequential GGS scheme for the MDO problem
  - MD feasible optimization solution,  $[O_1, O_2]$ :  $Z_{i,j} = H_{i,j}$
  - Single discipline feasible optimization solution,  $[O_1(A_1, S_1), O_2(A_2, S_2)]$ :

$$Z_{i,j} = \begin{pmatrix} R_{i,Q_j} & 0 & R_{i,b_j} \\ P_{i,Q_j} & P_{i,\Lambda_j} & P_{i,b_j} \\ g_{i,Q_j} & g_{i,\Lambda_j} & g_{i,b_j} \end{pmatrix}.$$

For all of these schemes an upper bound for the convergence factor is estimated by  $\mu \leq \sigma_1(\mathcal{M})$ , where  $\sigma_1$  denotes the maximal singular value of  $\mathcal{M}$ . In problems governed by PDEs the quantities  $\mathcal{M}$  are operators, typically non-differential, which measure the coupling between the disciplines in the problem.

The convergence theory was applied to two test cases: a system of two non-linear algebraic equations and a system of two PDEs which model an aeroelastic system (in both test cases there are non-linearities causing the coupling to be a local property). In both test cases MDA, MDS, and MDO problems were defined, analyzed, and tested numerically. In the first test case it is demonstrated how the convergence factors can be estimated in a finite dimensional level. In the second test case it is demonstrated how the convergence factors can be estimated in the PDE level; such estimates are expected to be more accurate as the discretization refines. The symbol of the convergence operators were computed explicitly and where estimated on the boundary (which is the interface between the two disciplines involved). The symbols indicate that the convergence operators are pseudo-differential and contain the information of the coupling between the two disciplines. We think that these operators play a major role in the theory of MDO governed by PDEs. The numerical results are compatible with the analytical estimates.

In applications, where large codes are involved, the different convergence factors can be approximated numerically, locally, using numerical computation (in the disciplinary level) of the Jacobians and Hessians of the different disciplines in the problem. These convergence factors can serve as a tool to develop algorithms for the solution of MD problems. When a problem is composed of more than two disciplines the convergence factor can be estimated between all the different disciplines. For example, if the problem is composed of three disciplines and the convergence factor of the iteration  $(A_1, A_2)$  and that of  $(A_1, A_3)$  is much smaller than that of  $(A_2, A_3)$ , then the scheme  $(A_1, [A_2, A_3])$  is expected to have desired convergence properties.

For MDO problems which have a “system level”, e.g., for  $O[(A_1, S_1), (A_2, S_2), (A_3, S_3)]$  the convergence theory can be applied to define algorithms for the solution of the MDA and MDS problems. Extension of this work to acceleration of MDO schemes will be discussed elsewhere.

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## REFERENCES

- [1] *5th AIAA/NASA/USAF/ISSMO Symposium on Multidisciplinary Analysis and Optimization*, Panama City, FL, Sept.7-9, (1994).
- [2] *6th AIAA/NASA/ISSMO Symposium on Multidisciplinary Analysis and Optimization*, Bellevue, WA, Sept.4-6, (1996).
- [3] N. ALEXANDROV AND M.Y.HUSSAINI, *Multidisciplinary Design Optimization - State of the Art*, Proceeding of the ICASE/NASA Langley Workshop on Multidisciplinary Design Optimization, SIAM (1997).
- [4] R.J. BALLING AND J. SOBIESKI, *Optimization of Coupled Systems: A Critical Overview of Approaches*. AIAA Paper 94-4330, 5th AIAA/NASA/USAF/ISSMO Symposium on Multidisciplinary Analysis and Optimization, Panama City, FL, Sept.7-9, (1994).
- [5] E. J. CRAMER, J. E. DENNIS, JR., P.D.FRANK, R.M.LEWIS AND G.R.SHUBIN, *Problem Formulation for Multidisciplinary Optimization*, SIAM J. Optimization, Vol. 4, No. 4, pp. 754-776, (1994).
- [6] G. R. SHUBIN, *Application of Alternative Multidisciplinary Optimization Formulations to a Model Problem for Static Aeroelasticity*, Journal of Computational Physics **118**, 73-85 (1995).
- [7] A. JAMESON, *Re-Engineering the Design Process through Computing*, AIAA-97-0641, 35th Aerospace Sciences Meeting & Exhibit, January 6-10, Reno, NV (1997).
- [8] I. KROO, *MDO for Large-Scale Design*, Multidisciplinary Design Optimization - State of the Art, Proceeding of the ICASE/NASA Langley Workshop on Multidisciplinary Design Optimization, SIAM (1997) p.22.
- [9] G. H. GOLUB AND C.F. VON LOAN, *Matrix Computation*, The John Hopkins University Press, (1989).
- [10] E. ARIAN, *Analysis of the Hessian for Aeroelastic Optimization*, ICASE report No. 95-84 (1995). *On the Coupling of Aerodynamic and Structural Design*, Journal of Computational Physics **135**, 83-96 (1997).
- [11] R. J. BALLING, *Approaches to MDO which support Disciplinary Autonomy*, Multidisciplinary Design Optimization - State of the Art, Proceeding of the ICASE/NASA Langley Workshop on Multidisciplinary Design Optimization, SIAM (1997) p.90.
- [12] J. L. LIONS, *Optimal Control of Systems Governed by Partial Differential Equations*, Translated by S.K.Mitter. Springer-Verlag, New York. (1971).
- [13] R. T. HAFTKA, *Second Order Design Derivatives in Structural Analysis*, AIAA J., **20**, 1765-1766 (1982).
- [14] E. LIVNE, *Integrated Multidisciplinary Aeroservoelastic Synthesis: Background, Progress, and Challenges*, Multidisciplinary Design Optimization - State of the Art, Proceeding of the ICASE/NASA Langley Workshop on Multidisciplinary Design Optimization, SIAM (1997) p.45.

- [15] L.N. TREFETHEN AND D. BAU, III, *Numerical Linear Algebra*, to be published by SIAM (1997).
- [16] E. J. HAUG, K. K. CHOI, AND V. KOMKOV, *Design Sensitivity Analysis of Structural Systems*, Vol. 177 of Mathematics in Science and Engineering, Academic Press, Orlando, FL (1986).
- [17] J. BORGGARD, *The Sensitivity Equation Method for Optimal Design*, Ph.D. Thesis. Virginia Tech, Blacksburg, VA (1994).
- [18] A. JAMESON, *Aerodynamic Design Via Control Theory*, ICASE report NO. 88-64, November (1988), Journal of Scientific Computing. **3**, 233 (1988).

**Appendix A. Norms.** Throughout the paper the  $L^2$  norm is used. In the following we define it for a vector, a matrix, a function, and a differential operator:

- Let  $\vec{u}$  be a vector in  $C^n$ , then

$$\|\vec{u}\|^2 = \vec{u}^T \cdot \vec{u},$$

- Let  $A$  be a matrix in  $C^{m \times n}$ , then,

$$\|A\| = \sup_{\vec{u} \in C^n} \frac{\|A\vec{u}\|}{\|\vec{u}\|},$$

- Let  $v = v(x)$  be a function in a Hilbert space  $\mathcal{H}$ , then

$$\|v\|^2 = \int v^2(x) dx,$$

- Let  $L$  be a differential operator  $L : \mathcal{H} \rightarrow \mathcal{W}$  where  $\mathcal{W}$  is a Hilbert space, then

$$\|L\| = \sup_{v(x) \in \mathcal{H}} \frac{\|Lv\|}{\|v\|}.$$

**Theorem** [15]

For any  $A \in C^{m \times n}$ , the  $L^2$  norm of  $A$  is given by

$$\|A\| = \sigma_1(A) = \rho^{\frac{1}{2}}(A^* A)$$

where  $\sigma_1$  is the maximal singular value and  $\rho$  is the spectral radius.

**Corollary**

Using the above theorem and Parseval's relation, the  $L^2$  norm of a differential operator can be bounded by

$$\|L\| \leq \max_k \rho^{\frac{1}{2}}(\hat{L}^*(k) \hat{L}(k)),$$

where  $\hat{L}(k)$  denotes the symbol of the operator  $L$ .

**Appendix B. The Sensitivity Equation and the Adjoint Methods.** Let  $L$  be a partial differential operator defining the following PDE:

$$L(Q, b_1, \dots, b_M) = 0,$$

where  $Q$  denotes the state variables and  $b_j$  denote the  $j$ 'th design variable. Let  $I = I(Q, b_1, \dots, b_M)$  be a functional. The sensitivity problem is to compute the derivatives

$$(B.1) \quad g_j = \frac{dI}{db_j}.$$

A brief summary of the “sensitivity equation method” (also known as “direct-differentiation”) and of the ”adjoint method” are given in the following. For a more extensive treatment of these methods see for example [16]-[17] for the sensitivity equation method and [12],[18] for the adjoint method.

**B.1. The Sensitivity Equation Method.** The sensitivity equations are a linear set of  $M$  equations given by

$$(B.2) \quad L_Q \psi_j + L_{b_j} = 0 \quad \text{for } 1 \leq j \leq M,$$

where the solutions  $\psi_j$  are the sensitivities of the state variables with respect to the design variables on all the domain:

$$(B.3) \quad \psi_j = \frac{dQ}{db_j}.$$

In terms of the sensitivities, the derivatives of the cost functional with respect to the design variables are given by

$$(B.4) \quad g_j = \frac{\partial I}{\partial Q} \psi_j + \frac{\partial I}{\partial b_j} \quad \text{for } 1 \leq j \leq M.$$

**B.2. The Adjoint Method.** With the adjoint method the computation of the derivatives  $g_j$  is done with the solution of only one linear PDE, rather than  $M$ , irrespective of the number of design variables.

The adjoint equation, for the adjoint variable  $\lambda$ , is a linear PDE is given by

$$(B.5) \quad L_Q^* \lambda + \frac{\partial I}{\partial Q} = 0.$$

where the operator  $L_Q^*$  is the adjoint of  $L_Q$ . In terms of the adjoint variable,  $\lambda$ , the derivatives of the cost functional with respect to the design variables are given by

$$(B.6) \quad g_j = L_{b_j}^* \lambda + \frac{\partial I}{\partial b_j}.$$

## Appendix C. Lemma 1.

### Lemma 1:

For a two states system (2.2), starting with errors  $\bar{Q}_1$  and  $\bar{Q}_2$  in the state variables and assuming that the errors satisfy the quasi-linear approximation (2.3), a GGS sequential iteration  $(A_1, A_2)$  results in the following error relations:

$$(C.1) \quad \begin{aligned} \bar{Q}_1^{n+1} &= \left( R_{1,Q_1}^{-1} R_{1,Q_2} (R_{2,Q_2}^{n-1})^{-1} R_{2,Q_1}^{n-1} \right) \bar{Q}_1 \\ \bar{Q}_2^{n+1} &= \left( R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} R_{1,Q_2} \right) \bar{Q}_2. \end{aligned}$$

### Proof:

The solution sequence  $(A_1, A_2)$  of system (2.2) implies first solving  $R_1$  for  $Q_1$  and then solving  $R_2$  for  $Q_2$  as defined in Eqs.(2.4-2.5). The solution of Eq.(2.5) is given by

$$(C.2) \quad \begin{pmatrix} \tilde{Q}_1 \\ \tilde{Q}_2 \end{pmatrix} = - \begin{pmatrix} R_{1,Q_1}^{-1} & 0 \\ -R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} & R_{2,Q_2}^{-1} \end{pmatrix} \begin{pmatrix} R_1 \\ R_2 \end{pmatrix}.$$

Let  $(Q_1^*, Q_2^*)$  denote the solution of the coupled system (2.2). The errors after a GGS iteration (2.4) are given by

$$(C.3) \quad \begin{aligned} \bar{Q}_1^{n+1} &= Q_1^* - (Q_1 + \tilde{Q}_1) = \bar{Q}_1 - \tilde{Q}_1 \\ \bar{Q}_2^{n+1} &= Q_2^* - (Q_2 + \tilde{Q}_2) = \bar{Q}_2 - \tilde{Q}_2. \end{aligned}$$

Substitution of (C.3) in (2.3) gives

$$(C.4) \quad \begin{pmatrix} R_{1,Q_1}^{n+1} & R_{1,Q_2}^{n+1} \\ R_{2,Q_1}^{n+1} & R_{2,Q_2}^{n+1} \end{pmatrix} \begin{pmatrix} \bar{Q}_1 - \tilde{Q}_1 \\ \bar{Q}_2 - \tilde{Q}_2 \end{pmatrix} = - \begin{pmatrix} R_1^{n+1} \\ R_2^{n+1} \end{pmatrix}.$$

Substitution of (C.2) in (C.4) gives

$$(C.5) \quad - \begin{pmatrix} R_1^{n+1} \\ R_2^{n+1} \end{pmatrix} = \begin{pmatrix} R_{1,Q_1}^{n+1} & R_{1,Q_2}^{n+1} \\ R_{2,Q_1}^{n+1} & R_{2,Q_2}^{n+1} \end{pmatrix} \mathcal{K} \begin{pmatrix} \bar{Q}_1 \\ \bar{Q}_2 \end{pmatrix}$$

where

$$(C.6) \quad \mathcal{K} = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} - \begin{pmatrix} R_{1,Q_1} & 0 \\ R_{2,Q_1} & R_{2,Q_2} \end{pmatrix}^{-1} \begin{pmatrix} R_{1,Q_1} & R_{1,Q_2} \\ R_{2,Q_1} & R_{2,Q_2} \end{pmatrix}.$$

Using relations (2.3) and multiplication of Eq.(C.5) from the left by the matrix

$$\begin{pmatrix} R_{1,Q_1}^{n+1} & R_{1,Q_2}^{n+1} \\ R_{2,Q_1}^{n+1} & R_{2,Q_2}^{n+1} \end{pmatrix}^{-1}$$

results in the following relation between the errors before and after a GGS iteration for MDA:

$$(C.7) \quad \begin{pmatrix} \bar{Q}_1^{n+1} \\ \bar{Q}_2^{n+1} \end{pmatrix} = \left[ \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} - \begin{pmatrix} R_{1,Q_1}^{-1} & 0 \\ -R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} & R_{2,Q_2}^{-1} \end{pmatrix} \begin{pmatrix} R_{1,Q_1} & R_{1,Q_2} \\ R_{2,Q_1} & R_{2,Q_2} \end{pmatrix} \right] \begin{pmatrix} \bar{Q}_1 \\ \bar{Q}_2 \end{pmatrix}$$

From Eq.(C.7) it is concluded that

$$(C.8) \quad \begin{aligned} \bar{Q}_1^{n+1} &= -(R_{1,Q_1})^{-1} R_{1,Q_2} \bar{Q}_2 \\ \bar{Q}_2^{n+1} &= R_{2,Q_2}^{-1} R_{2,Q_1} R_{1,Q_1}^{-1} R_{1,Q_2} \bar{Q}_2. \end{aligned}$$

By the above two relations the following holds:

$$(C.9) \quad \bar{Q}_1^{n+1} = - \left( R_{1,Q_1}^{-1} R_{1,Q_2} \right) \left( (R_{2,Q_2}^{n-1})^{-1} R_{2,Q_1}^{n-1} (R_{1,Q_1}^{n-1})^{-1} R_{1,Q_2}^{n-1} \right) \bar{Q}_2^{n-1}$$

and

$$(C.10) \quad \bar{Q}_1 = - \left( (R_{1,Q_1}^{n-1})^{-1} R_{1,Q_2}^{n-1} \right) \bar{Q}_2^{n-1}.$$

Substituting  $\bar{Q}_2^{n-1}$  of relation (C.10) in relation (C.9) results in an expression for the error reduction in  $Q_1$ :

$$(C.11) \quad \bar{Q}_1^{n+1} = \left( R_{1,Q_1}^{-1} R_{1,Q_2} (R_{2,Q_2}^{n-1})^{-1} R_{2,Q_1}^{n-1} \right) \bar{Q}_1.$$

□

## Appendix D. Fourier Analysis of the Aeroelastic Problem.

**D.1. The Analysis Problem.** The error equations are analyzed with Fourier analysis resulting in the symbols of the Jacobian operators,  $R_{i,Q_j}$ . Then Parseval's relation is applied to estimate the norm of the operators  $R_{i,Q_j}$  in the real space.

The Flow Analysis Problem:  $R_1(\phi, \beta) = 0$

The analysis problem,  $R_1$ , is given by the following PDE (in this specific case the error equation is identical to the state equation):

$$(D.1) \quad \begin{aligned} \Delta\phi &= 0 & \text{in } \Omega &= \{0 < x < 1 ; 0 < y < 1\} \\ \partial_z\phi &= \beta & \text{on } z &= 0 \\ \partial_x\phi &= 0 & \text{on } x &= 0 \\ \partial_x\phi &= 0 & \text{on } x &= 1 \\ \phi &= 0 & \text{on } z &= 1 \end{aligned}$$

where  $\beta = \beta(x)$  is some non-constant  $L^2[0, 1]$  function.

The solution of Eq.(D.1) is given by

$$(D.2) \quad \phi(x, z) = \sum_{k=-\infty, k \neq 0}^{\infty} \frac{\hat{\beta}_k}{2\pi k} \psi_k(z) e^{i(2\pi k x)}$$

where

$$(D.3) \quad \psi_k(z) = -\tanh(2\pi k) \cosh(2\pi k z) + \sinh(2\pi k z).$$

Since the function  $|\psi_k(z)|$  has a maximum at  $z = 0$  in the interval  $z \in [0, 1]$ , for all  $k$ , we conclude that

$$(D.4) \quad |\phi(x, z)| \leq |\phi(x, 0)| \quad 0 \leq z \leq 1$$

and therefore, for the sake of error convergence, we will examine the error in  $\phi$  on the boundary only ( $z = 0$ ).

By Eq.(D.2) on the boundary  $\phi = \phi(x)$  satisfies

$$(D.5) \quad \begin{aligned} \phi(x, 0) &= -\sum_{k=-\infty, k \neq 0}^{\infty} \hat{\beta}_k \frac{\tanh(2\pi k)}{2\pi k} e^{i(2\pi k x)} \\ \phi_z(x, 0) &= \sum_{k=-\infty, k \neq 0}^{\infty} \hat{\beta}_k e^{i(2\pi k x)}. \end{aligned}$$

We conclude the following symbols of the Jacobians:

$$(D.6) \quad \begin{aligned} \hat{R}_{1,\phi}(k) &= -\frac{2\pi k}{\tanh(2\pi k)} & \hat{R}_{1,W}(k) &= -2\pi i k \\ \hat{R}_{1,\alpha}(k) &= -2\pi i k & \hat{R}_{1,D}(k) &= 0. \end{aligned}$$

The Structure Analysis Problem:  $R_2(W, D) = 0$

The analysis problem,  $R_2$ , is given by the following PDE (simply supported boundary conditions):

$$(D.7) \quad \begin{aligned} \partial_{xx}(D\partial_{xx}W) &= -p & \text{on } z &= 0 ; 0 < x < 1 \\ W(0) &= W(1) = 0 \\ \partial_{xx}W(0) &= \partial_{xx}W(1) = 0. \end{aligned}$$

Linearization of (D.7) results in the following error equation

$$(D.8) \quad \begin{aligned} \partial_{xx}(\bar{D}\partial_{xx}W) + \partial_{xx}(D\partial_{xx}\bar{W}) &= -\bar{p} \quad \text{on } z=0 ; 0 < x < 1 \\ \bar{W}(0) &= \bar{W}(1) = 0 \\ \partial_{xx}\bar{W}(0) &= \partial_{xx}\bar{W}(1) = 0. \end{aligned}$$

The errors  $\bar{W}$ ,  $\bar{D}$ , and  $\bar{p}$  are expanded by a Fourier series:

$$(D.9) \quad \bar{W}(x) = \sum_{k=-\infty, k \neq 0}^{\infty} \hat{W}_k e^{i(2\pi kx)} \quad ; \quad \bar{D}(x) = \sum_{k=-\infty, k \neq 0}^{\infty} \hat{D}_k e^{i(2\pi kx)} \quad ; \quad \bar{p}(x) = \sum_{k=-\infty, k \neq 0}^{\infty} \hat{p}_k e^{i(2\pi kx)}.$$

Substitution of (D.9) into (D.8) results in an expression for the symbol of  $R_2$ :

$$(D.10) \quad \hat{R}_2 = \hat{G}_W(D)\hat{W} + \hat{G}_D(W)\hat{D} + \hat{p}_\phi\hat{\phi}$$

where

$$(D.11) \quad \begin{aligned} \hat{G}_W(D) &= D(2\pi k)^4 - 2i(\partial_x D)(2\pi k)^3 - (\partial_{xx} D)(2\pi k)^2 \\ \hat{G}_D(W) &= -(2\pi k)^2 \partial_{xx} W + 2(2\pi i k) \partial_{xxx} W + \partial_{xxxx} W \\ \hat{p}_\phi &= 2\pi i k. \end{aligned}$$

Therefore, the symbols of the Jacobians are give by

$$(D.12) \quad \begin{aligned} \hat{R}_{2,\phi}(k) &= 2\pi i k \quad ; \quad \hat{R}_{2,W}(k) = \hat{G}_W(D) \\ \hat{R}_{2,\alpha}(k) &= 0 \quad ; \quad \hat{R}_{2,D}(k) = \hat{G}_D(W). \end{aligned}$$

## D.2. The Adjoint Problem.

### The Adjoint Flow Problem

The symbol of the adjoint flow operator  $P_1$  on the boundary is given by  $(P_1(\lambda, \eta, \phi, W) = \partial_z \lambda - \partial_x \eta - 2\gamma_1 \partial_{xx} \phi - \gamma_3 \partial_x W)$

$$(D.13) \quad \hat{P}_1(k) = -\frac{2\pi k}{\tanh(2\pi k)} \hat{\lambda} - (2\pi i k) (\hat{\eta} + \gamma_3 \hat{W}) + 2\gamma_1 (2\pi k)^2 \hat{\phi},$$

therefore the symbols of the Jacobians are given by

$$(D.14) \quad \begin{aligned} \hat{P}_{1,\phi}(k) &= 2\gamma_1 (2\pi k)^2 & \hat{P}_{1,W}(k) &= -\gamma_3 (2\pi i k) \\ \hat{P}_{1,\lambda}(k) &= -\frac{2\pi k}{\tanh(2\pi k)} & \hat{P}_{1,\eta}(k) &= -2\pi i k \\ \hat{P}_{1,\alpha}(k) &= 0 & \hat{P}_{1,D}(k) &= 0. \end{aligned}$$

### The Adjoint Structure Problem

The symbol of the adjoint structure operator  $P_2$  on the boundary is given by  $(P_2(\lambda, \eta, \phi, D) = \partial_{xx}(D\partial_{xx}\eta) + \partial_x \lambda + \gamma_3 \partial_x \phi)$

$$(D.15) \quad \hat{P}_2(k) = \hat{G}_W(D)\hat{\eta} + \hat{G}_D(\eta)\hat{D} + (2\pi i k)(\hat{\lambda} + \gamma_3 \hat{\phi}),$$

therefore the symbols of the Jacobians are given by

$$(D.16) \quad \begin{aligned} \hat{P}_{2,\phi}(k) &= \gamma_3 (2\pi i k) & \hat{P}_{2,W}(k) &= 0 \\ \hat{P}_{2,\lambda}(k) &= 2\pi i k & \hat{P}_{2,\eta}(k) &= \hat{G}_W(D) \\ \hat{P}_{2,\alpha}(k) &= 0 & \hat{P}_{2,D}(k) &= \hat{G}_D(\eta). \end{aligned}$$



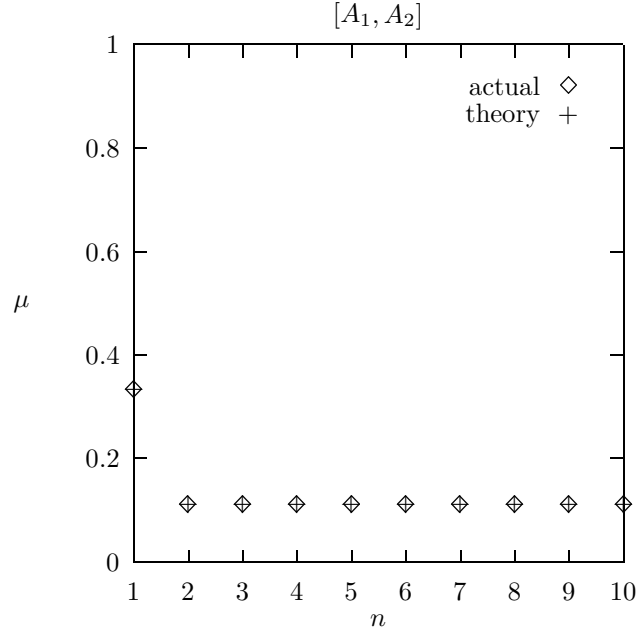


FIG. 6. Actual convergence rate versus theoretical upper bound for the GGS (sequential) solution of the non-linear algebraic system.

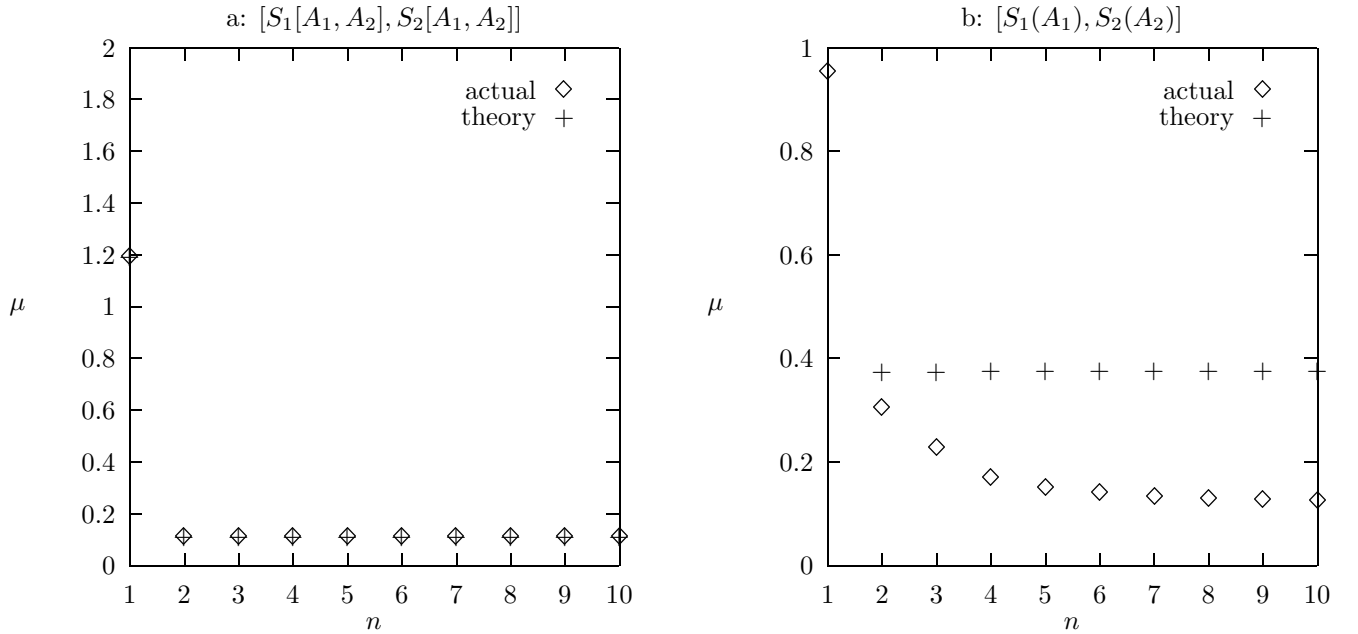


FIG. 7. Actual convergence rate versus theoretical upper bound for the MD feasible (left) and single discipline feasible (right) sensitivity Solution of the non-linear algebraic system.

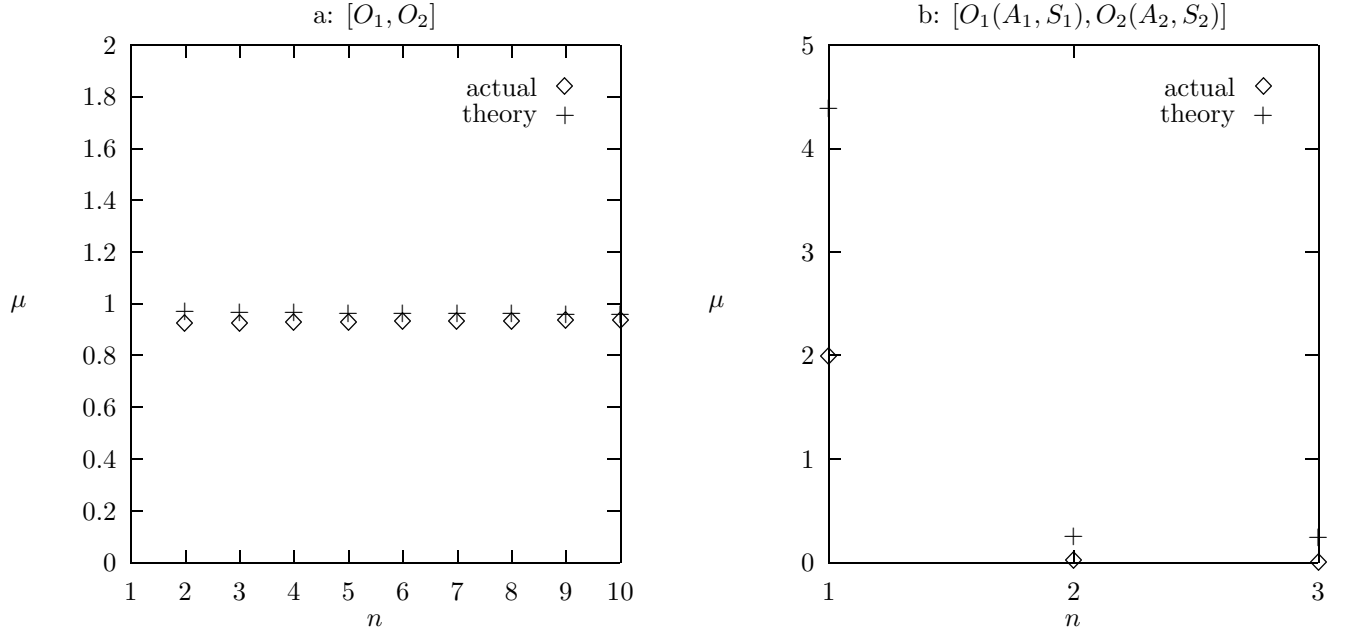


FIG. 8. Actual convergence rate versus theoretical upper bound for the MD feasible (left) and single discipline feasible (right) optimization solution of the non-linear algebraic system.

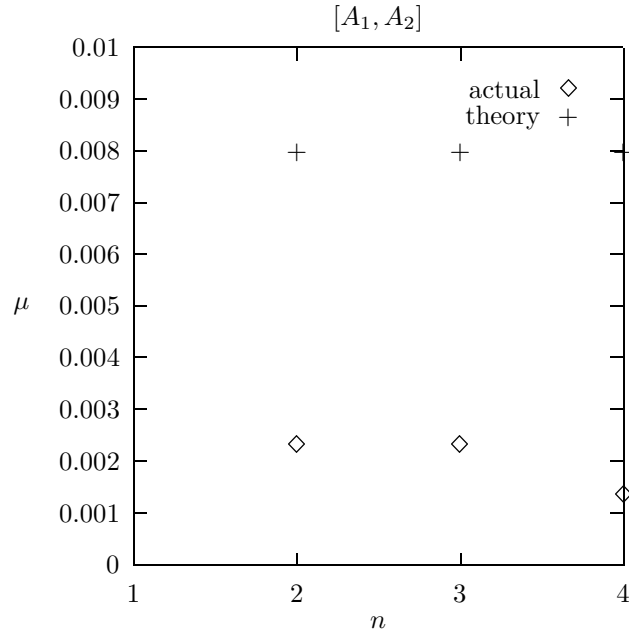


FIG. 9. Actual convergence rate versus theoretical upper bound for the GGS (sequential) solution of the aeroelastic problem.

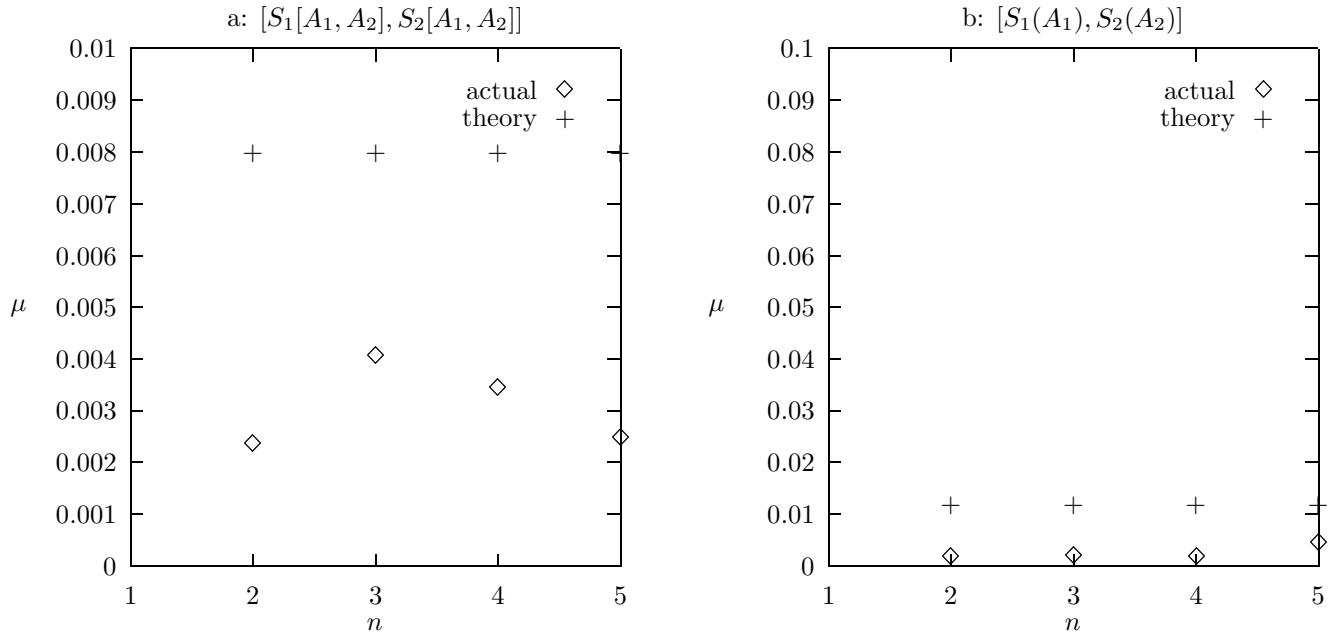


FIG. 10. Actual convergence rate versus theoretical upper bound for the MD feasible (left) and single discipline feasible (right) sensitivity solution of the aeroelastic problem.

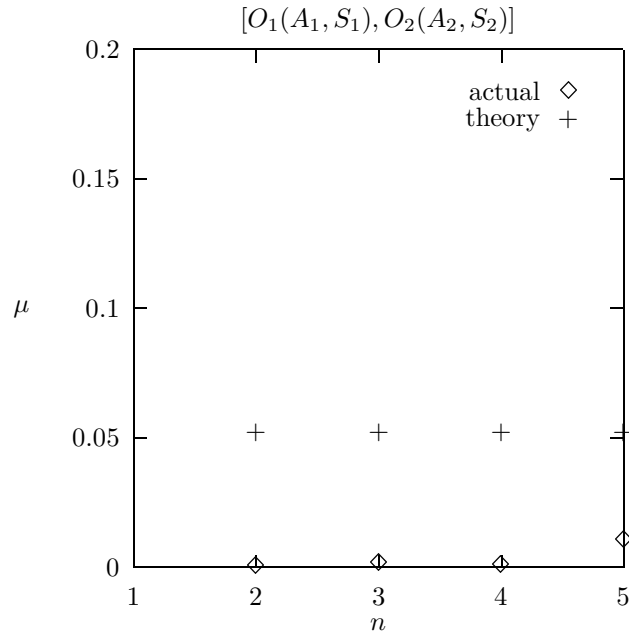


FIG. 11. Actual convergence rate versus theoretical upper bound for the single discipline feasible optimization solution of the aeroelastic problem.